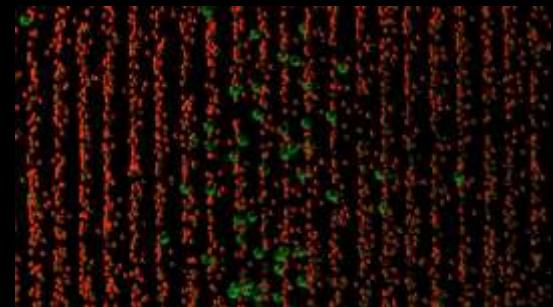


Metastability Alloy Design

D. Raabe, D. Ponge



**Max-Planck-Institut
für Eisenforschung GmbH**
Düsseldorf, Germany





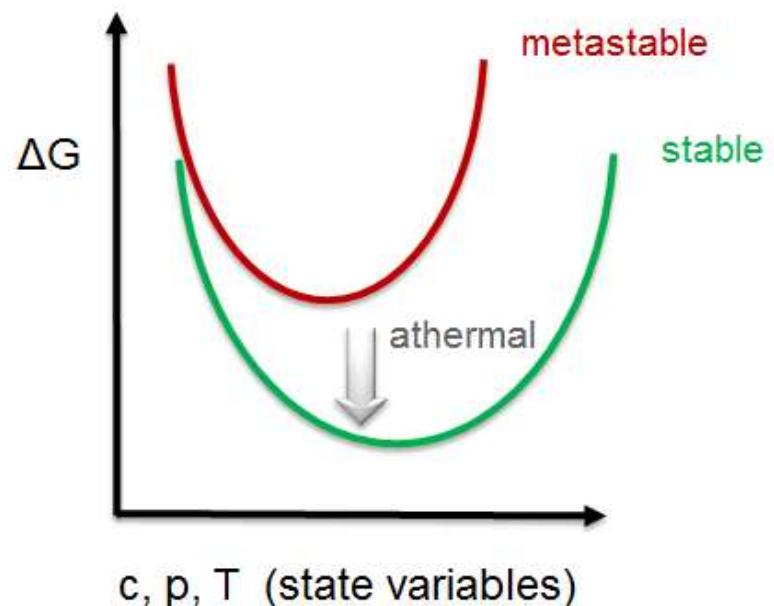
1. What is Metastability Alloy Design and Segregation Engineering ?

2. How is it done ?

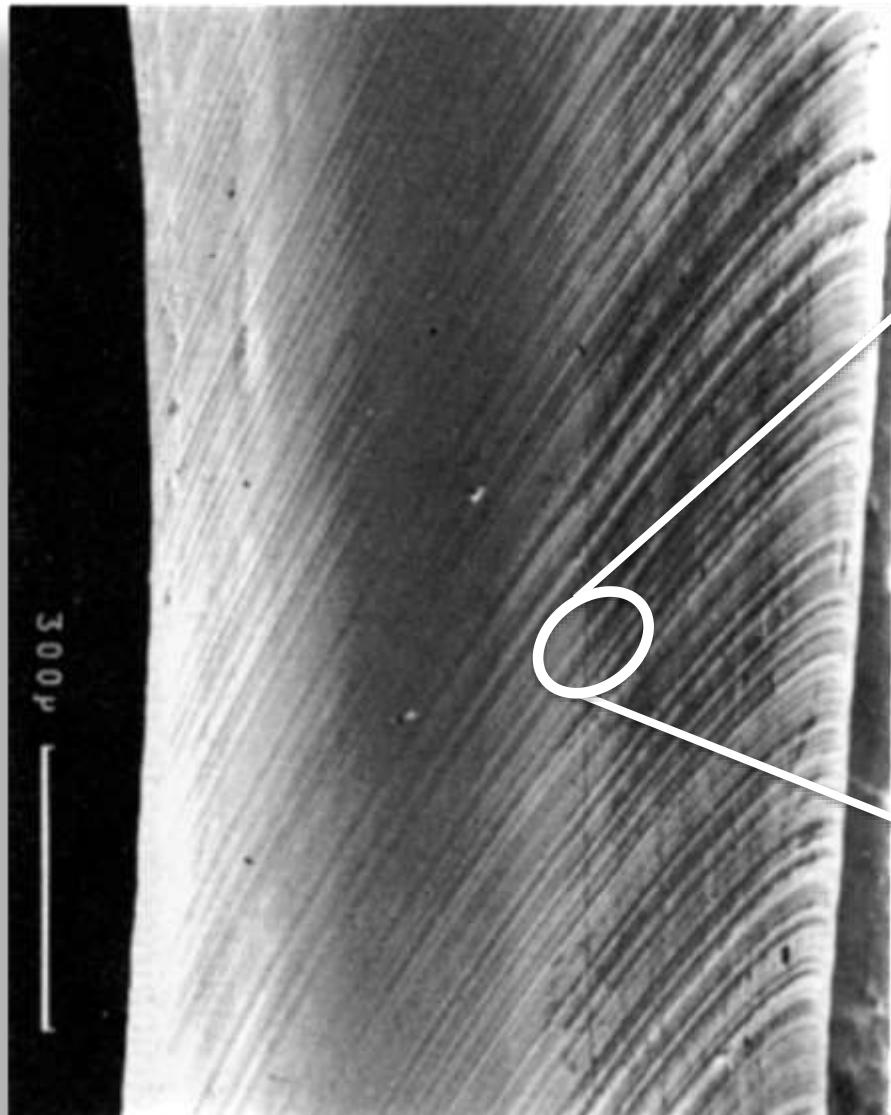


Chemo-mechanical metastability of crystalline phases

Displacive phase transformation under load



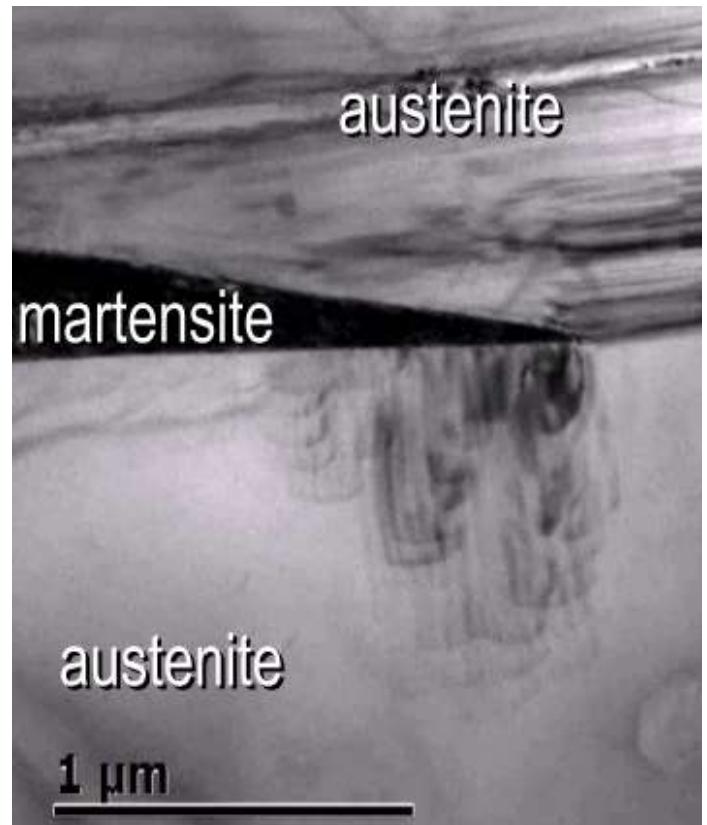
Plastic deformation and strength through dislocation slip



TEM: J. Kacher

**Athermal transformations not affine,
not commensurate -
high misfit deformation**

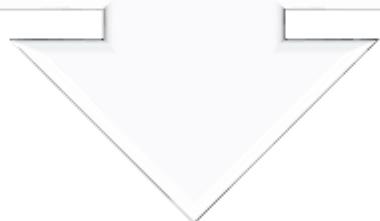
Multiple strain hardening effects



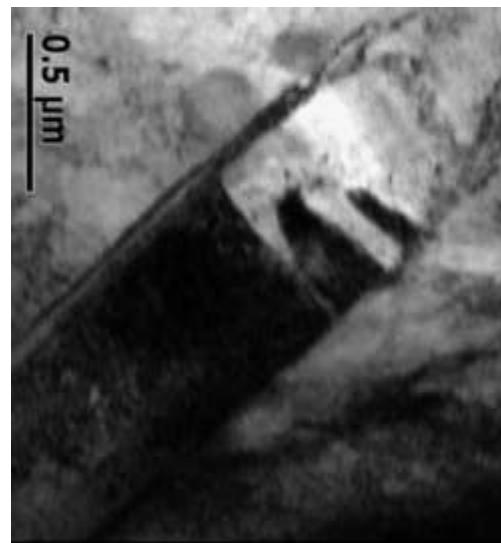
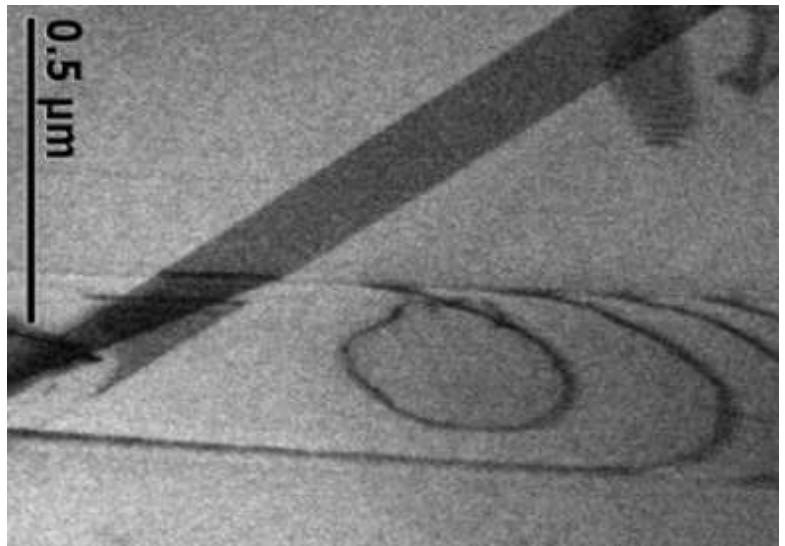


Chemo-mechanical metastability of crystals

Displacive phase transformation under load



Confined at lattice defects using chemical and size effects



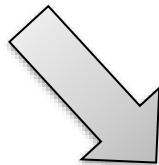


1. What is Metastability Alloy Design and Segregation Engineering ?

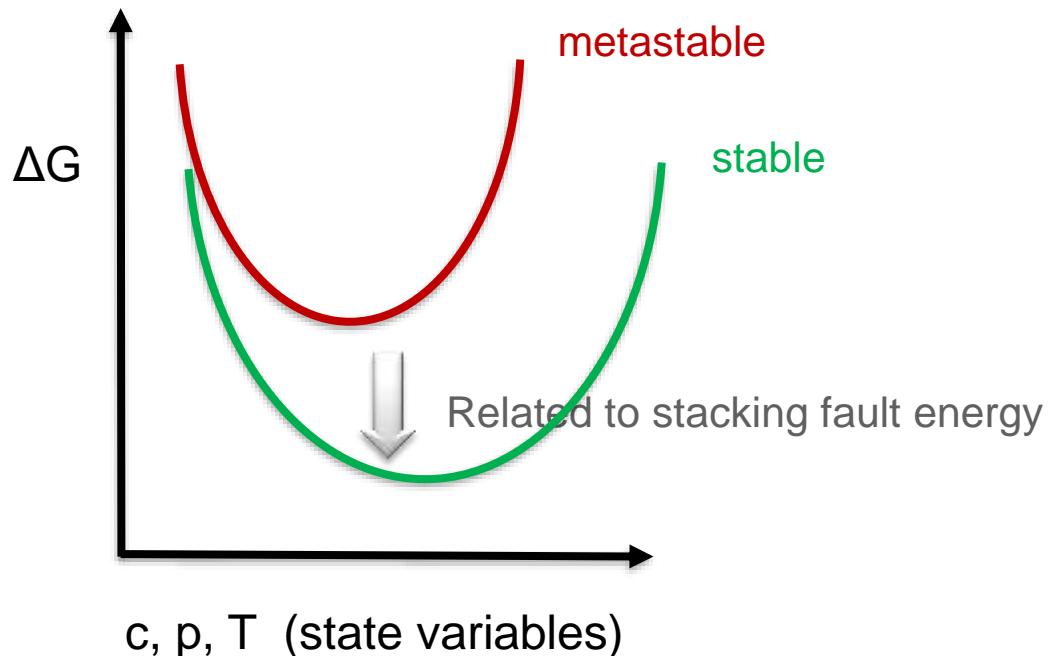
2. How is it done ?

1. What is Metastability Alloy Design and Segregation Engineering ?

2. How is it done ?



- Bulk: tune barriers & transformation driving forces
- Confinement to lattice defects
Segregation & local displacive transformation



- Bulk: tune barriers & transformation driving forces
- Confinement to lattice defects
Segregation & local displacive transformation

Bulk metastability FCC alloy design: tune stacking fault energy



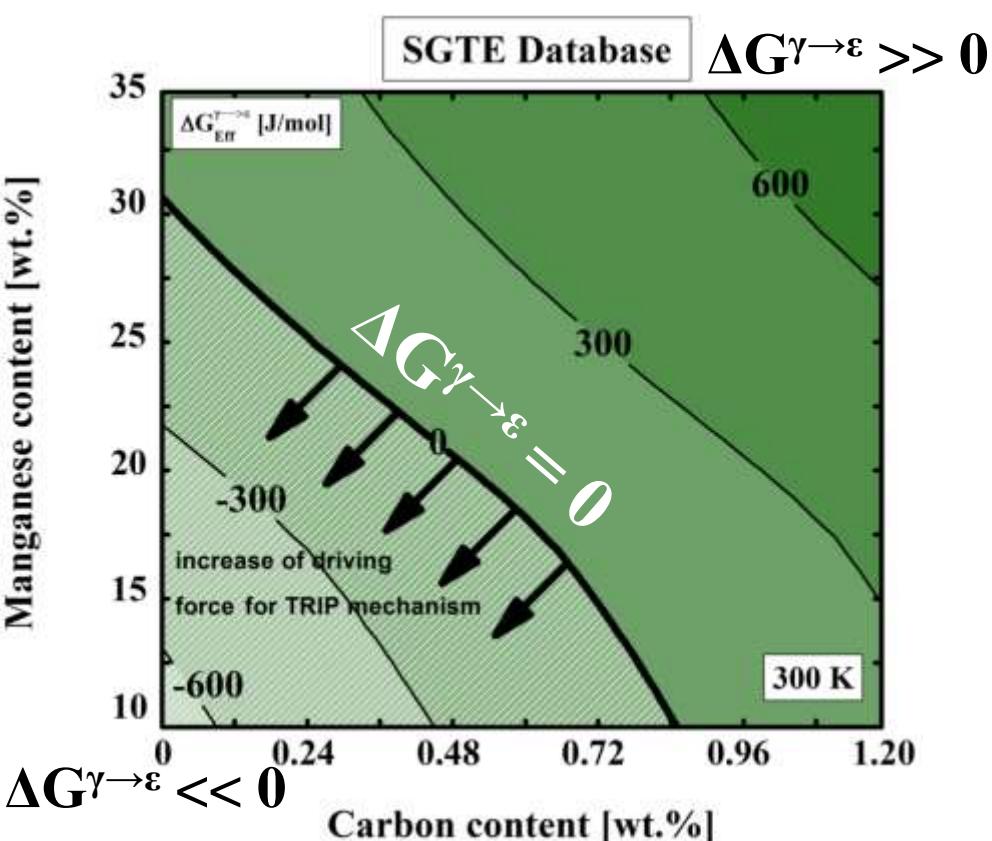
lower SFE

high-Mn (15-30%), HEA

γ (fcc) cells \rightarrow γ (fcc) planar \rightarrow γ (fcc+order) planar \rightarrow γ (fcc+twins) \rightarrow ε (hcp) \rightarrow α' (bcc/ bct)

high-Mn+Al

medium-Mn (5-12%)



Critical stress for twin growth:

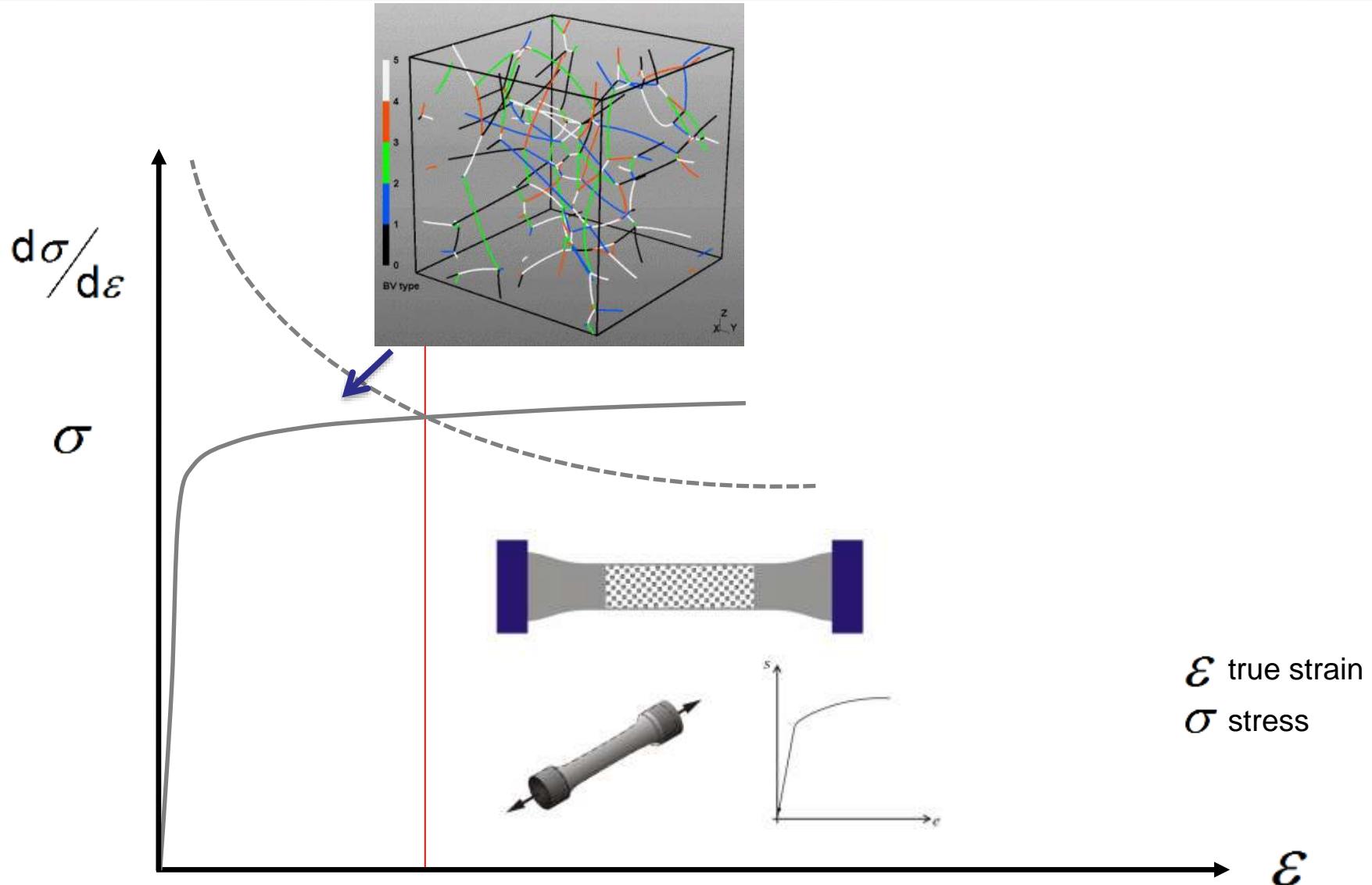
$$\tau_c = \frac{\gamma_{sf}}{3b_s} + \frac{3Gb_s}{L_0}$$

Critical stress for ε -martensite growth:

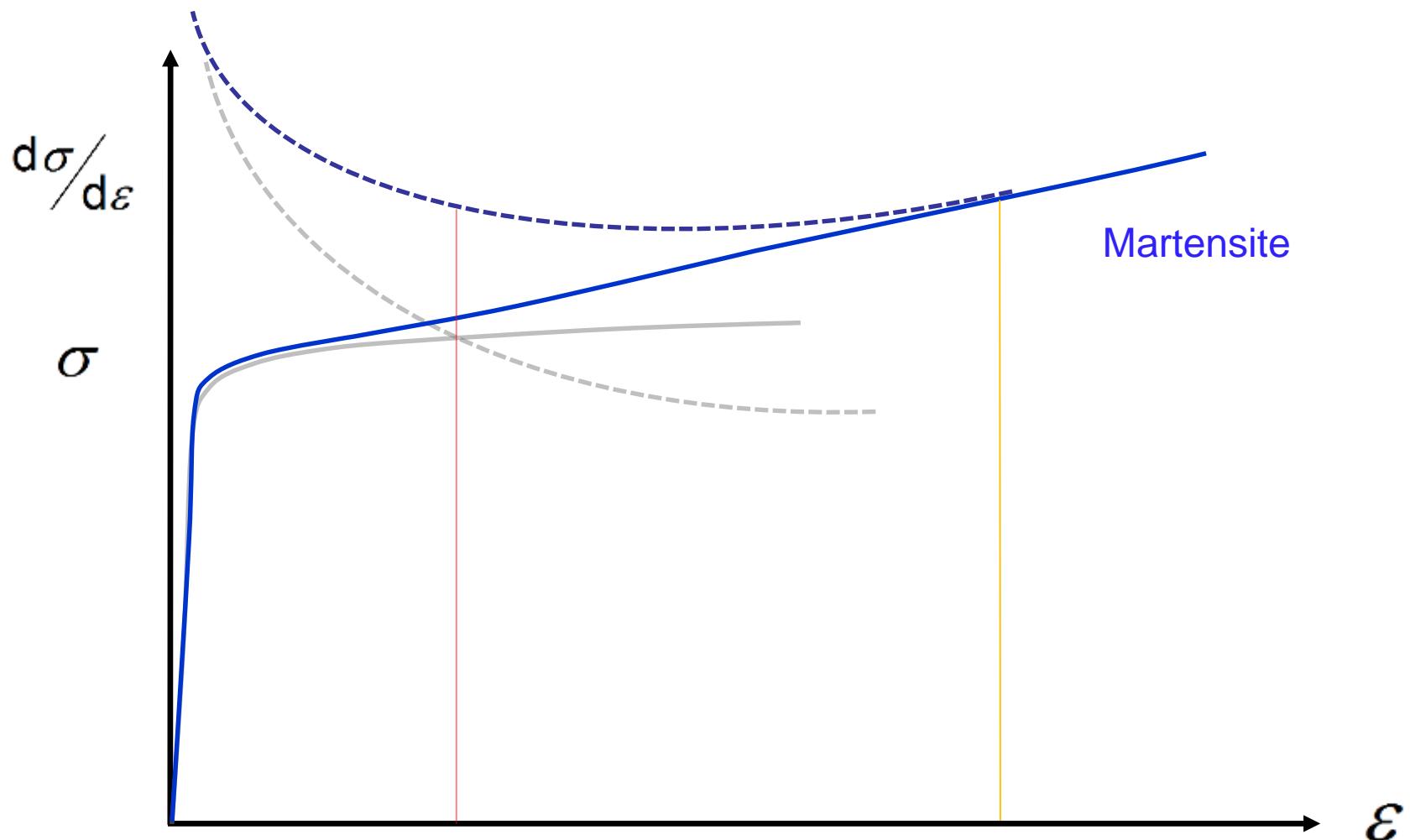
$$\tau_c = \frac{\gamma_{sf}}{3b_s} + \frac{3Gb_s}{L_0} + \frac{h\Delta G^{\gamma \rightarrow \varepsilon}}{3b_s}$$

Values of SFEs: D. Pierce, Acta Mater 68 (2014)

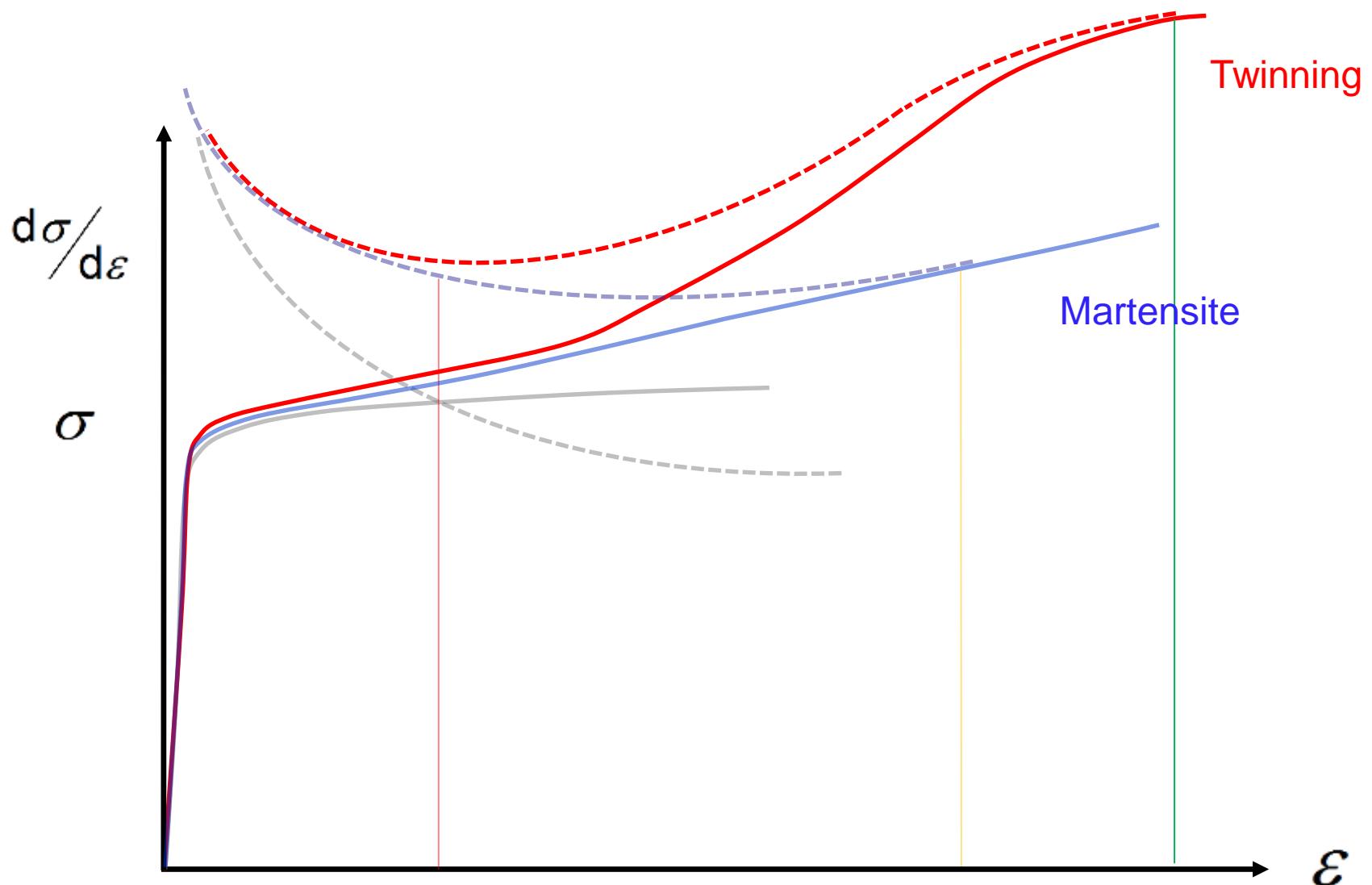
Inverse strength-ductility: phenomenological analysis



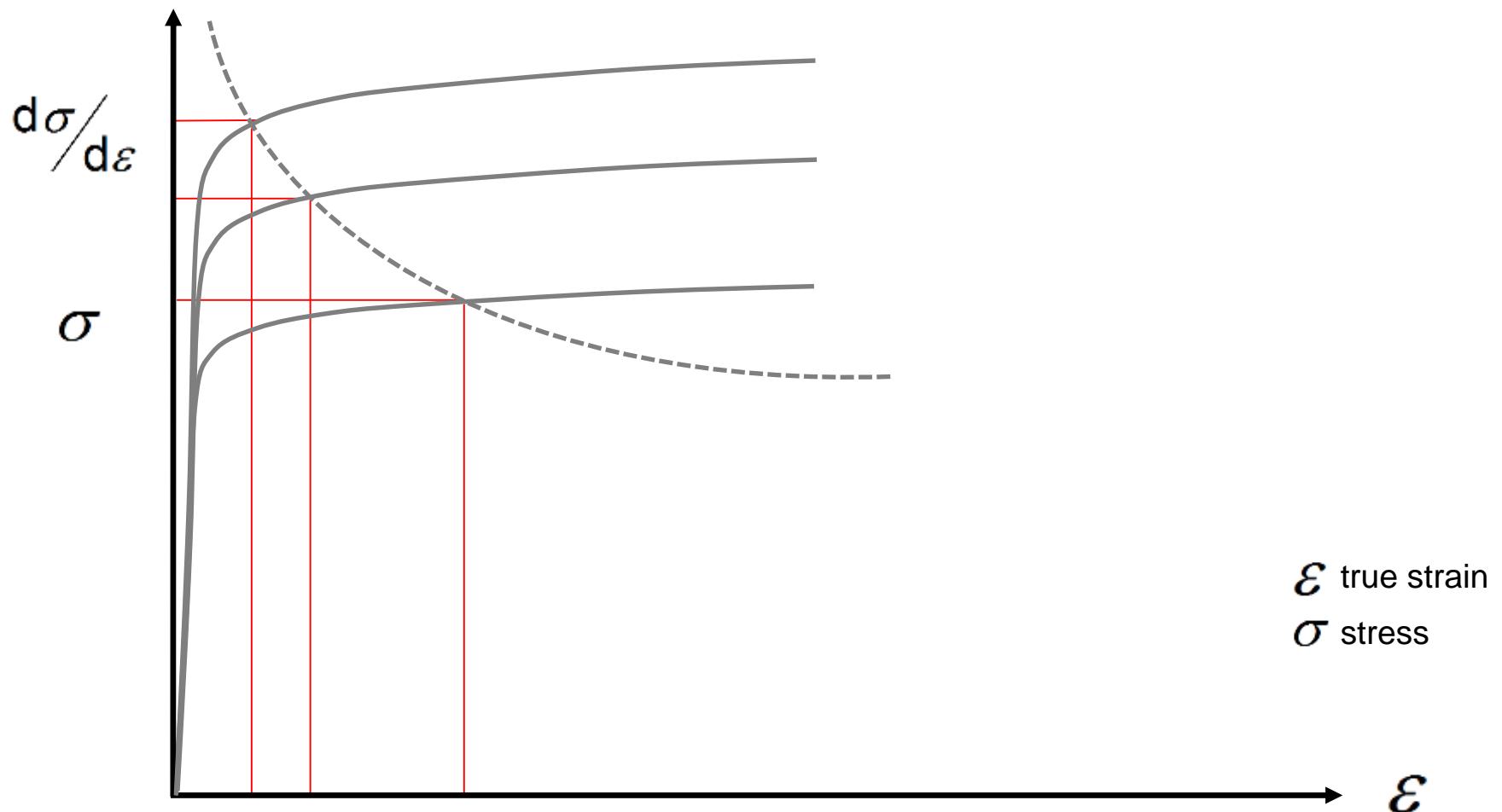
Inverse strength-ductility: phenomenological analysis



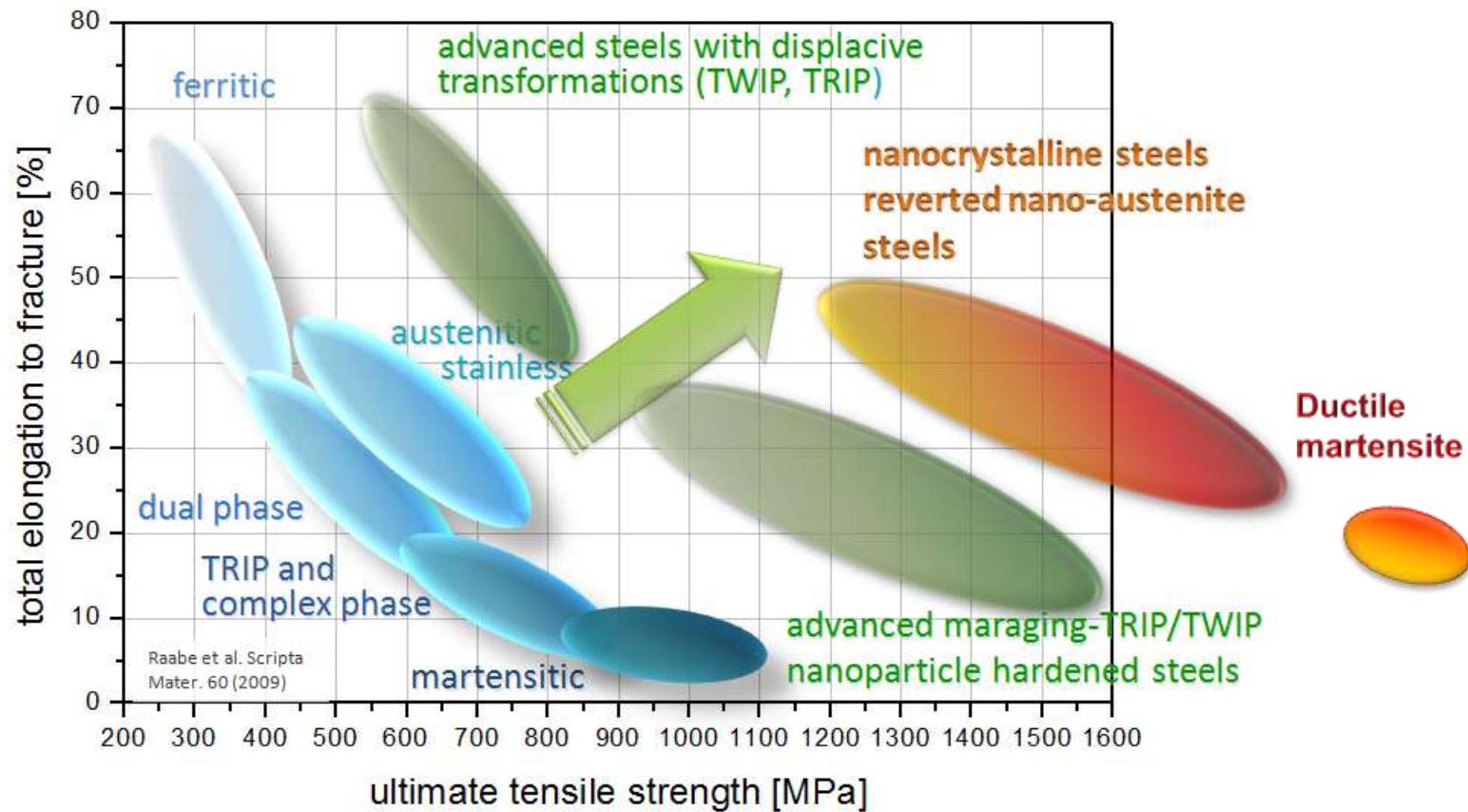
Inverse strength-ductility: phenomenological analysis



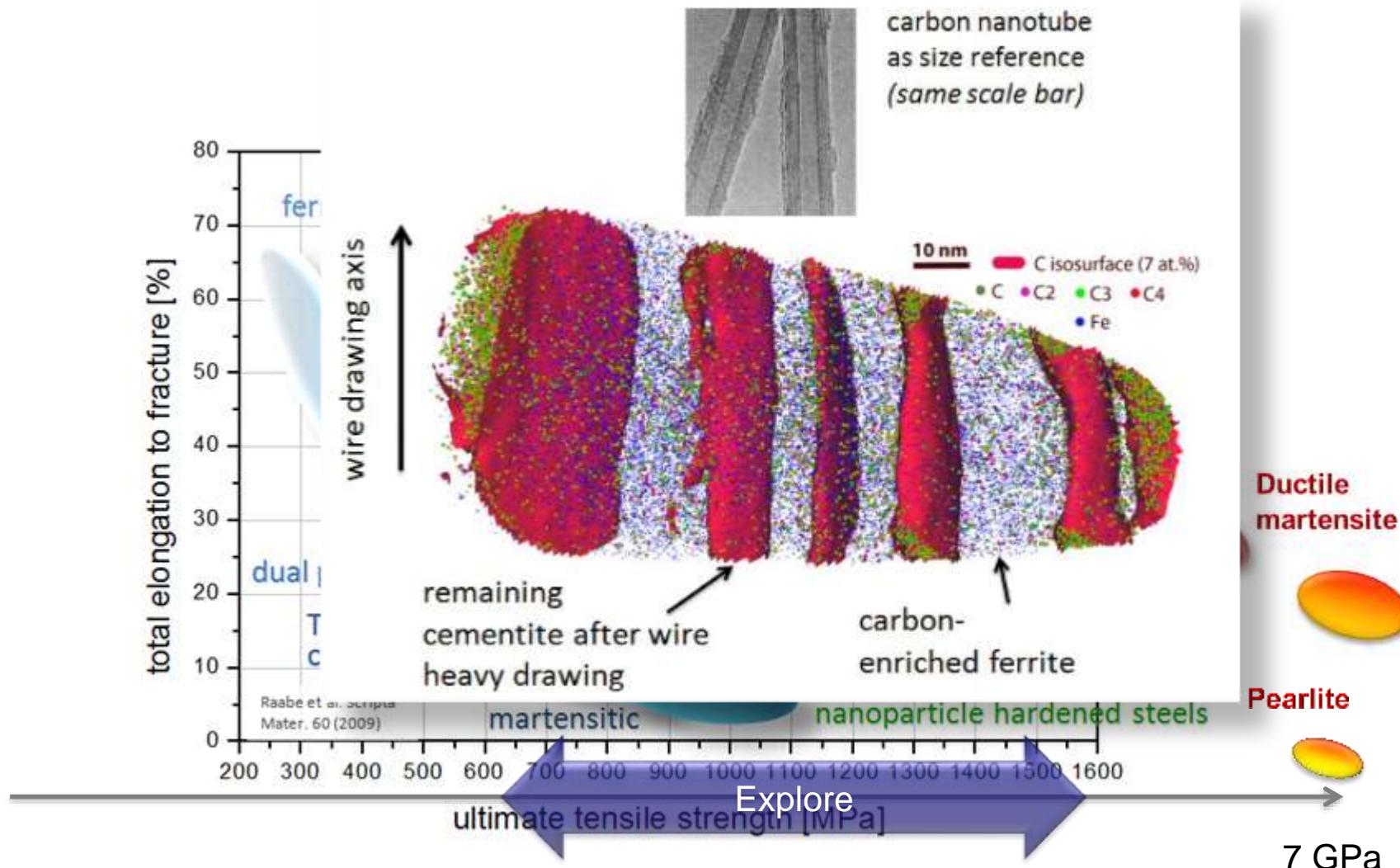
Inverse strength-ductility: phenomenological analysis



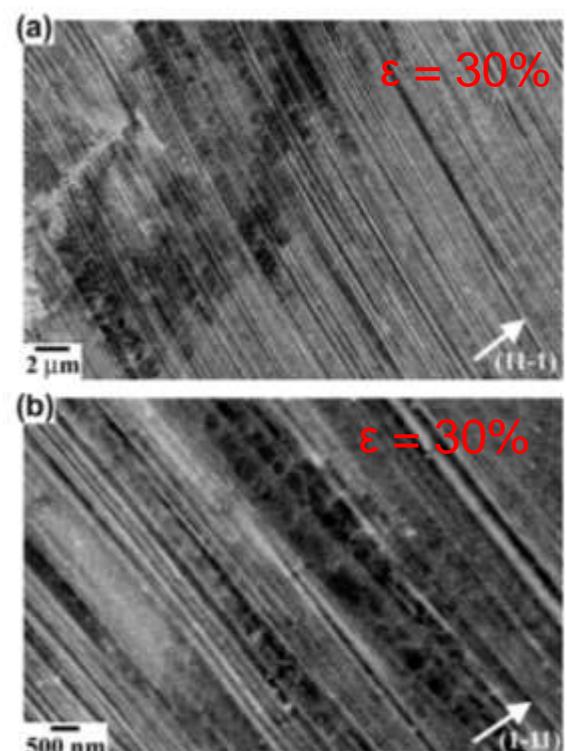
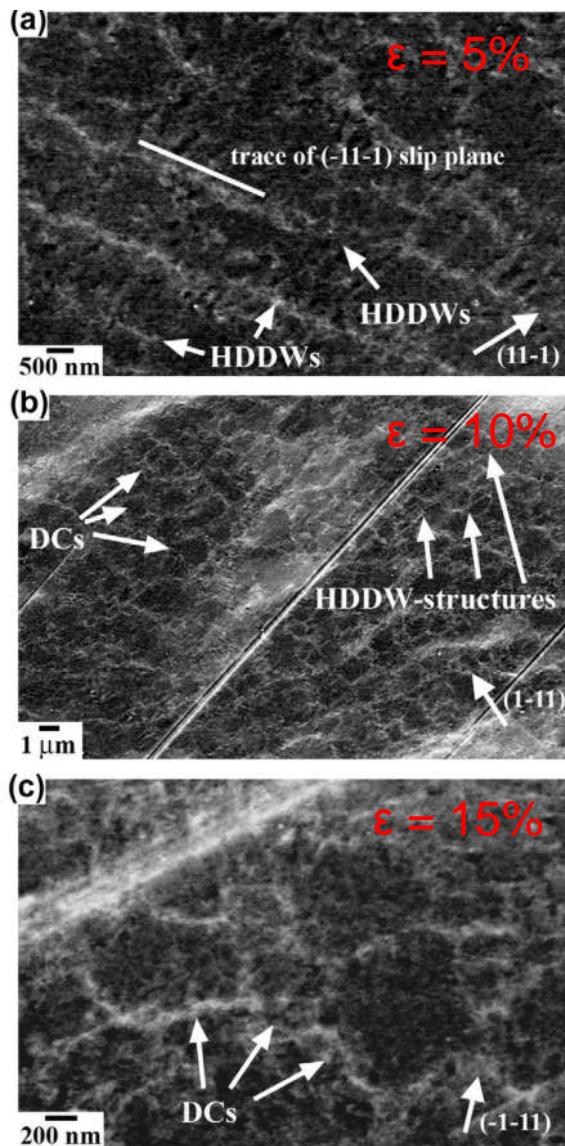
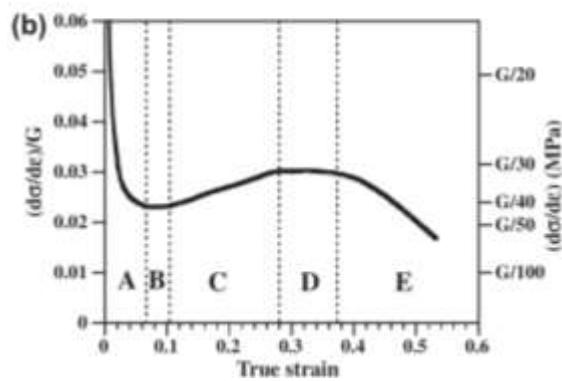
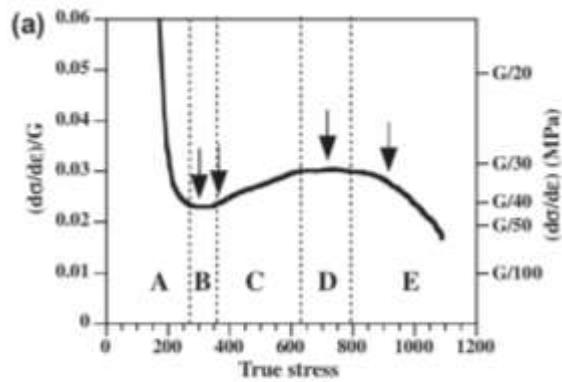
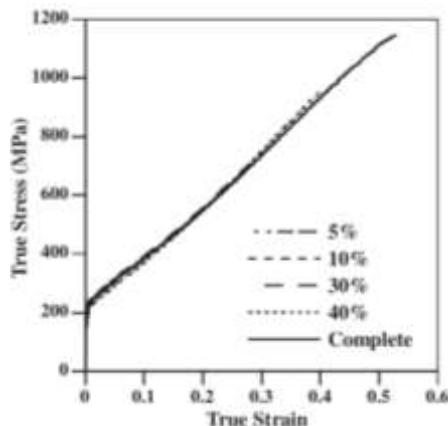
Metastability and segregation design: strengthening mechanisms



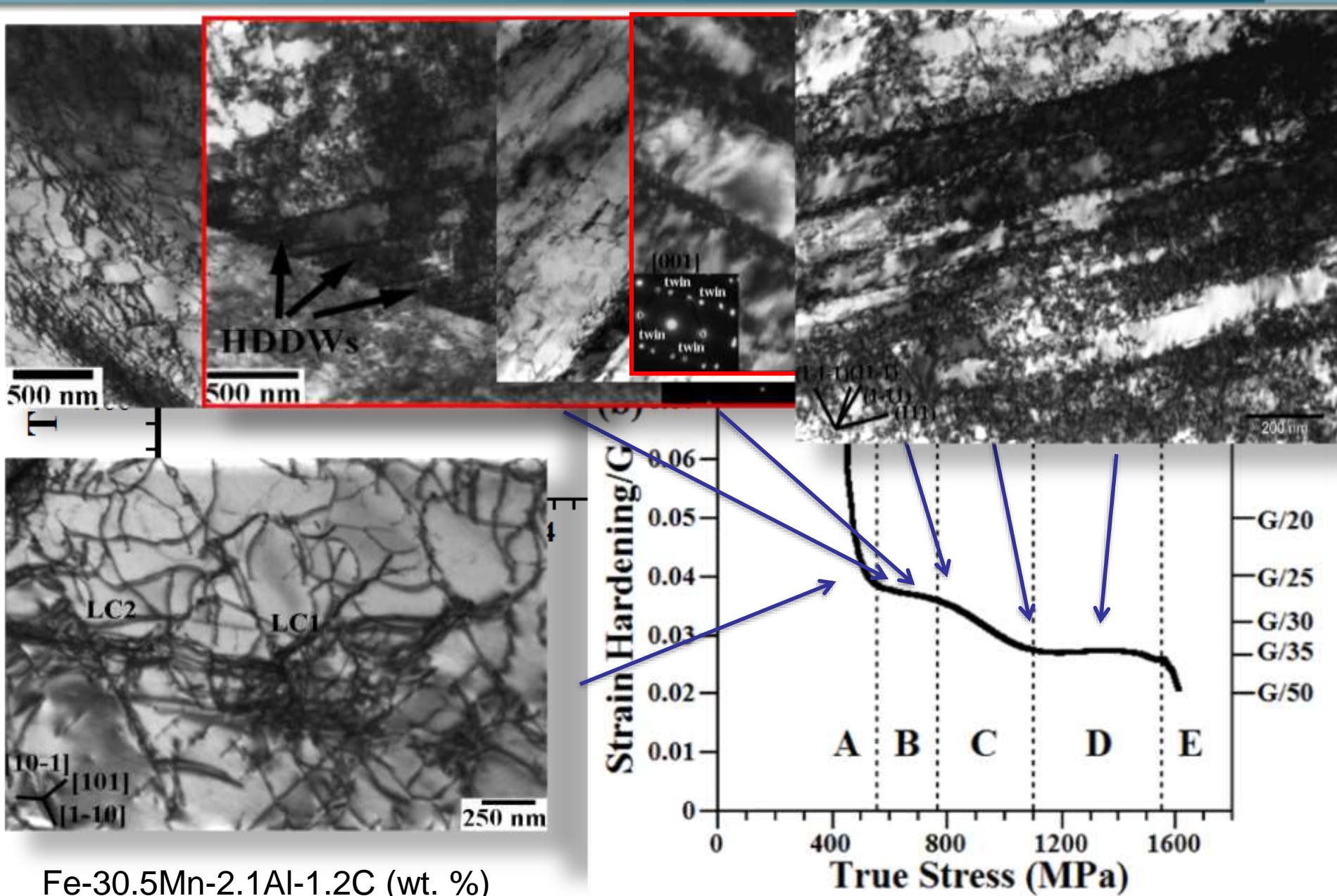
Metastability Alloy Design: strengthening mechanisms



Bulk Metastability Alloy Design: Fe-22Mn-0.6C TWIP steel (wt.%)



Bulk Metastability Alloy Design: Fe-Mn-Al-C solid solution



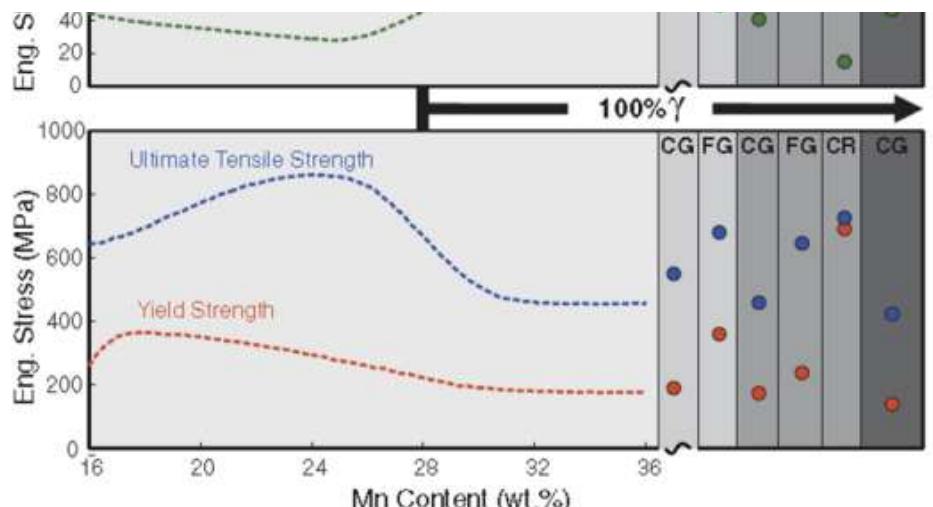
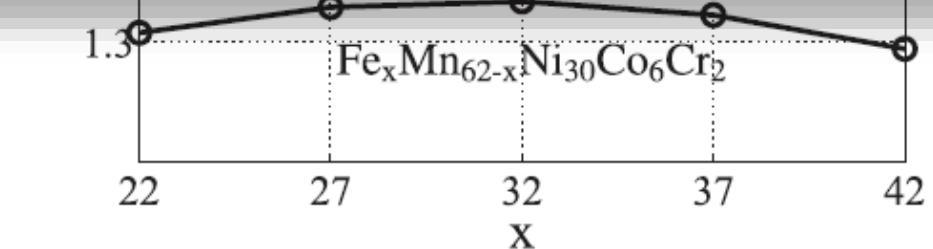
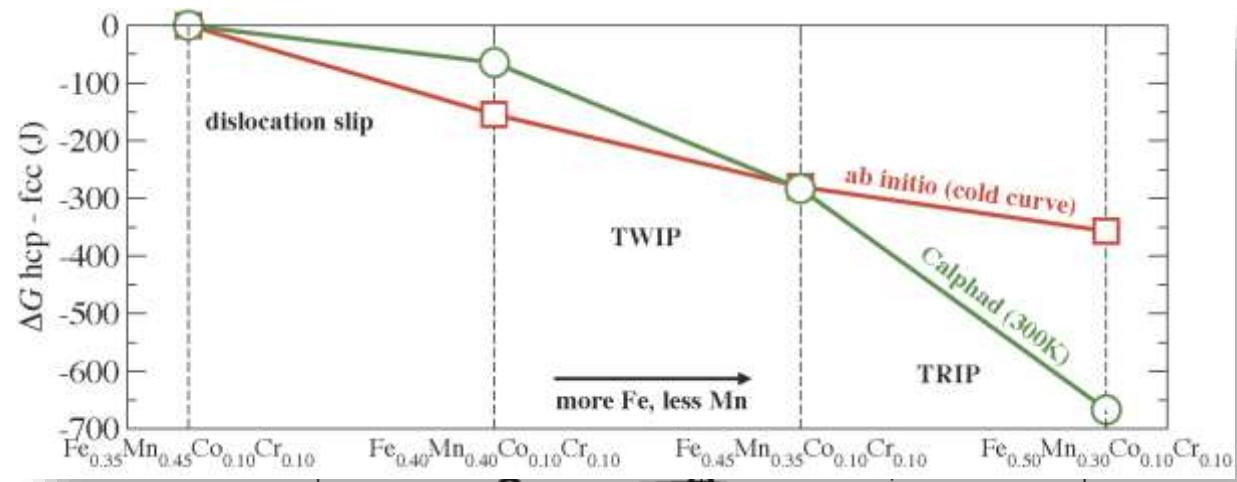
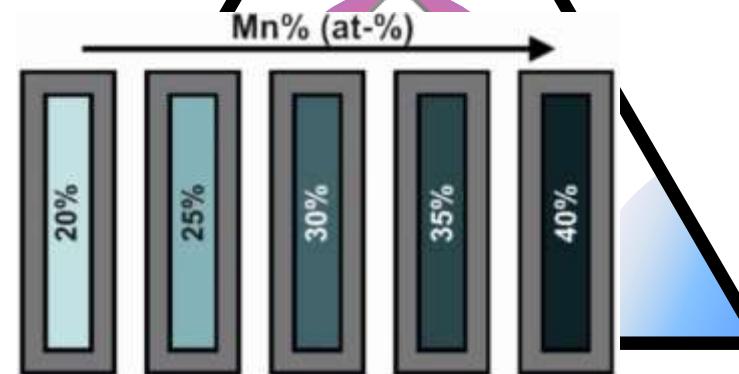
Motivation for non-equiautomic HEAs: FeMnNiCoCr (Cantor alloy)



Not only driven by config. entropy
Flat entropy curve

Phase stability and SFE
Drop single phase rule

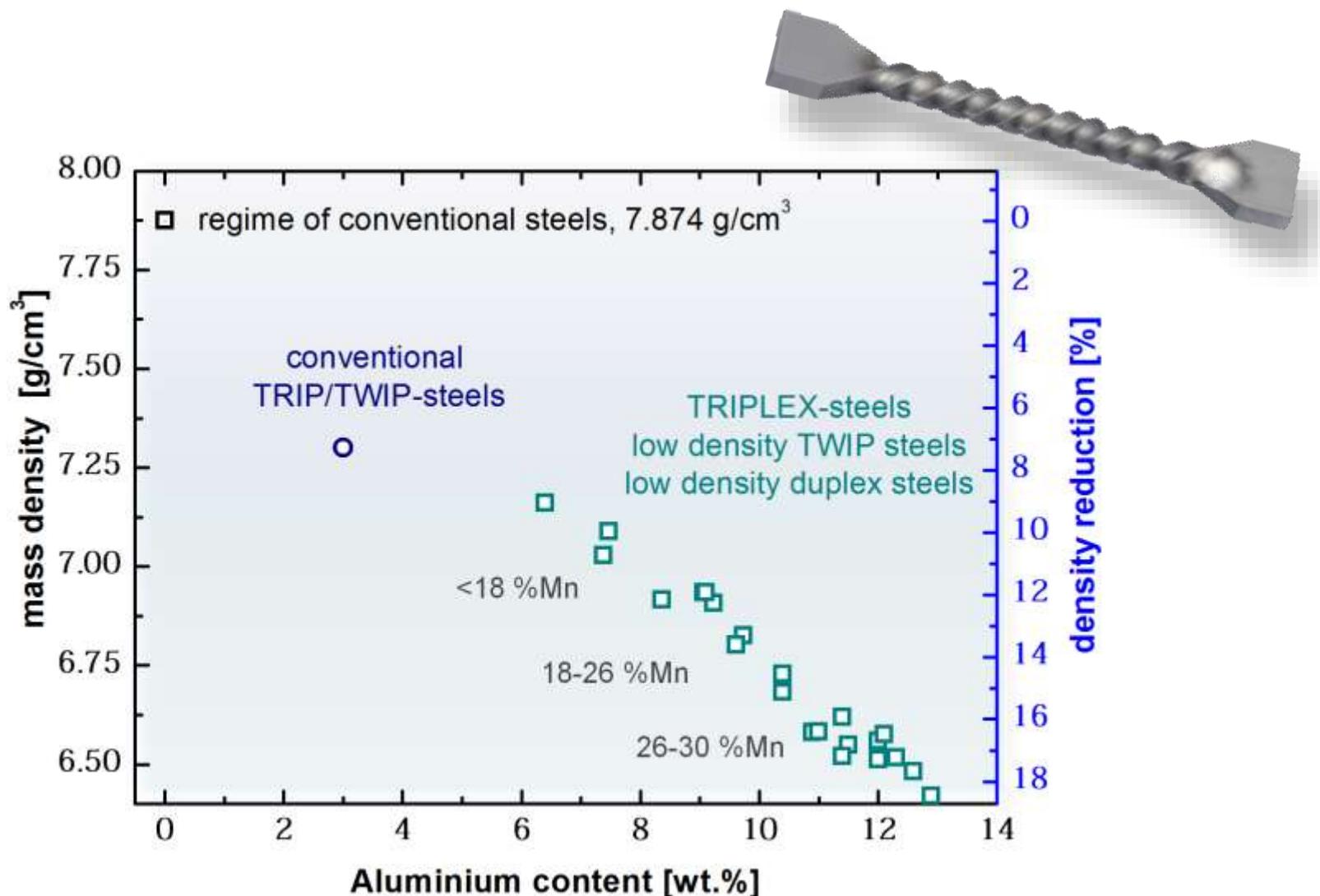
Bulk Rapid Alloy Prototyping: RAP
Property maps



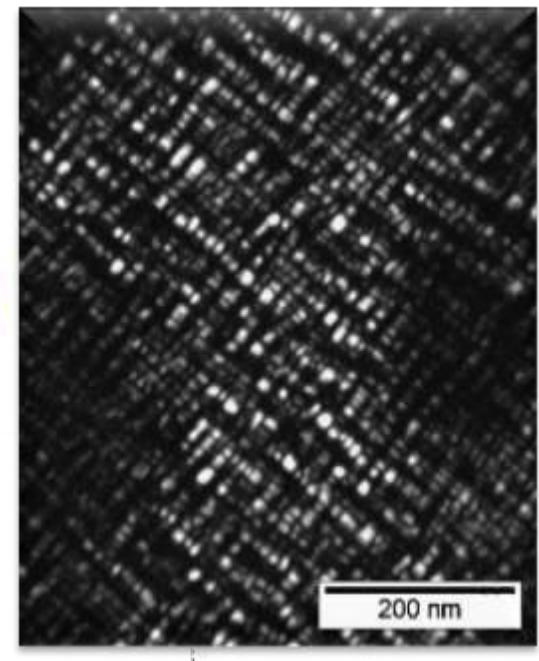
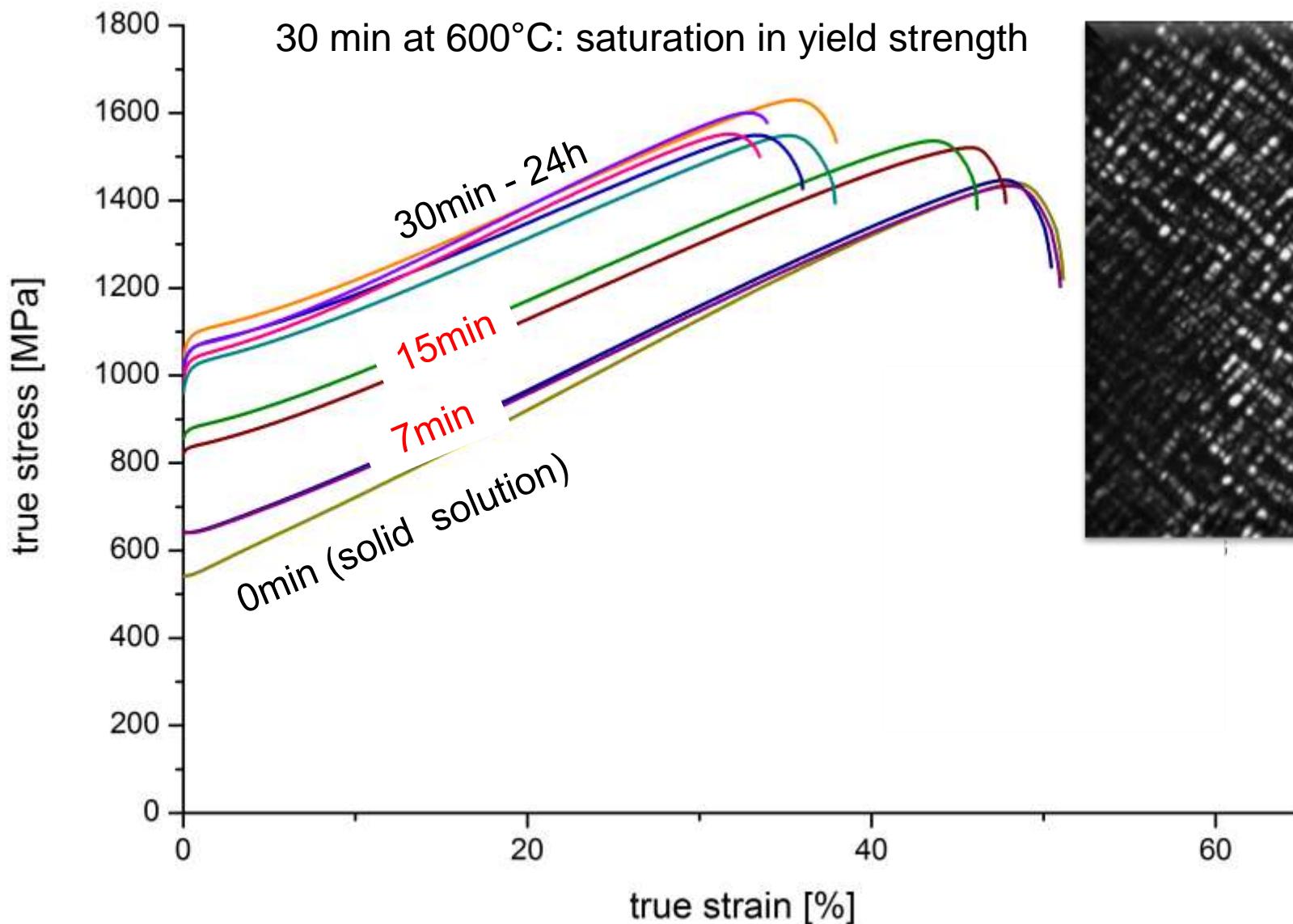
H. Springer et al. Acta Mater. 60 (2012) 4950

D. Ma et al. Acta Mater. 100 (2015) 90

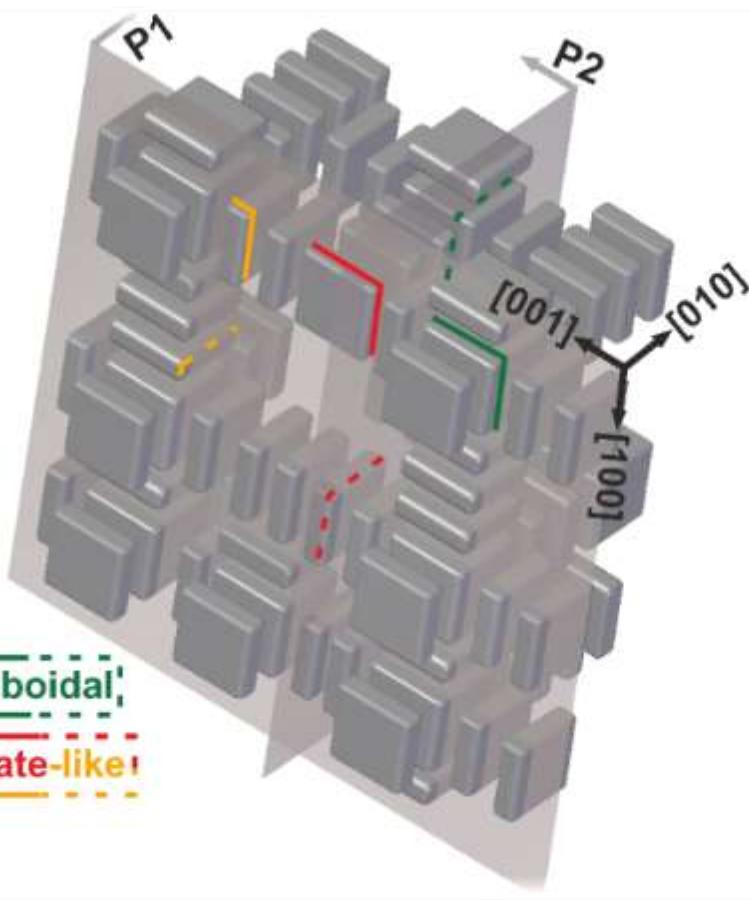
Example: Fe-Mn-Al-C alloys – 10-18% weight reduction



Fe-30Mn-8Al-1.2C, different annealing times at 600°C



γ/κ steel Fe-30Mn-8Al-1.2C

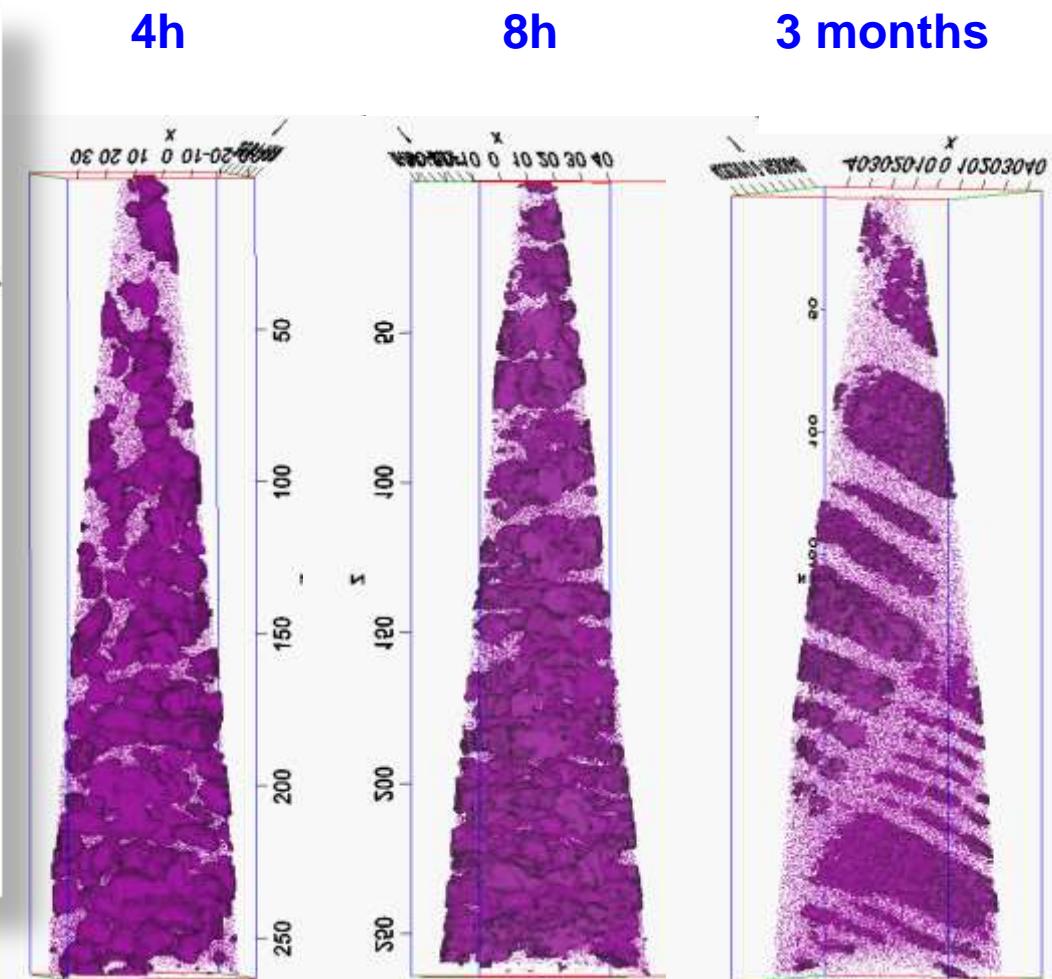


cuboidal

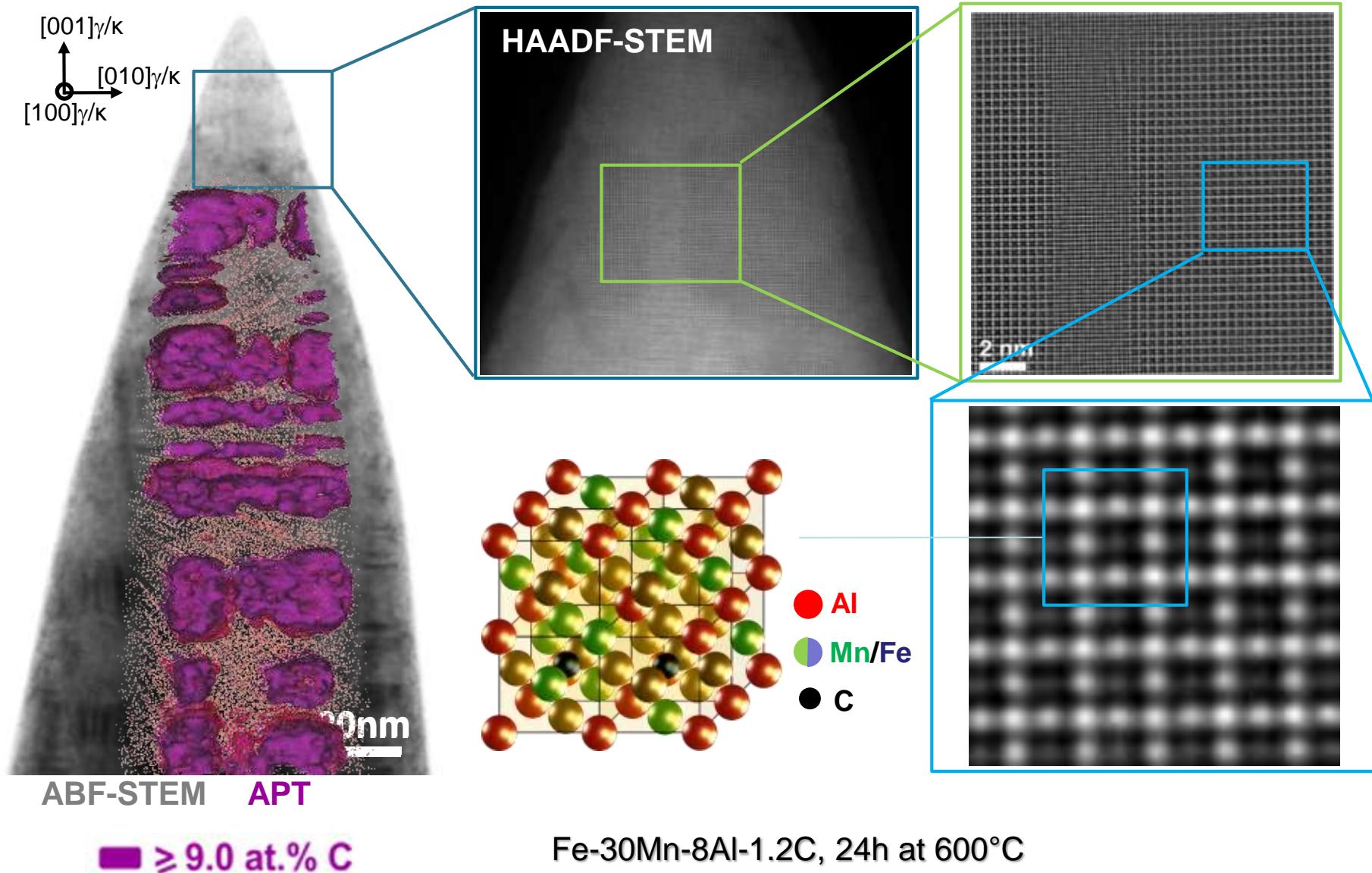
plate-like

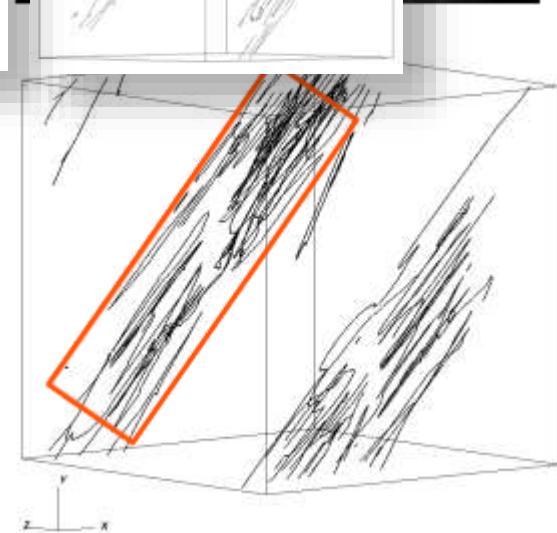
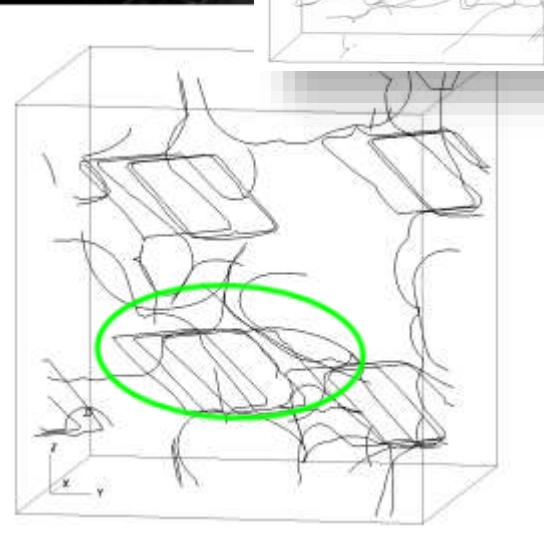
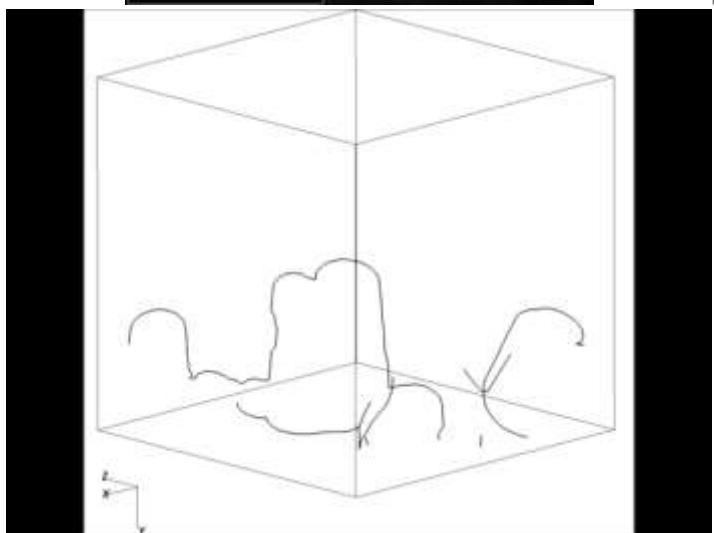
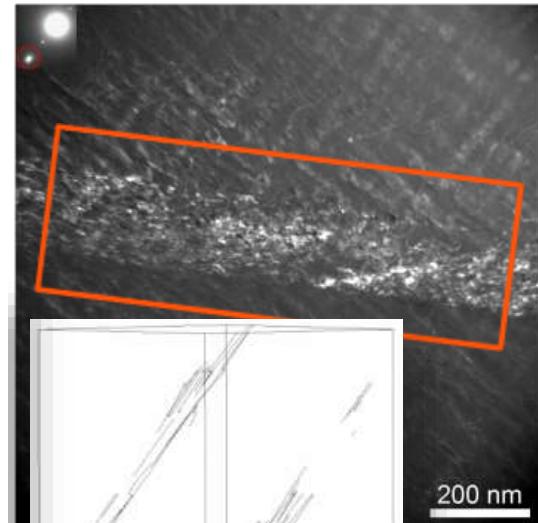
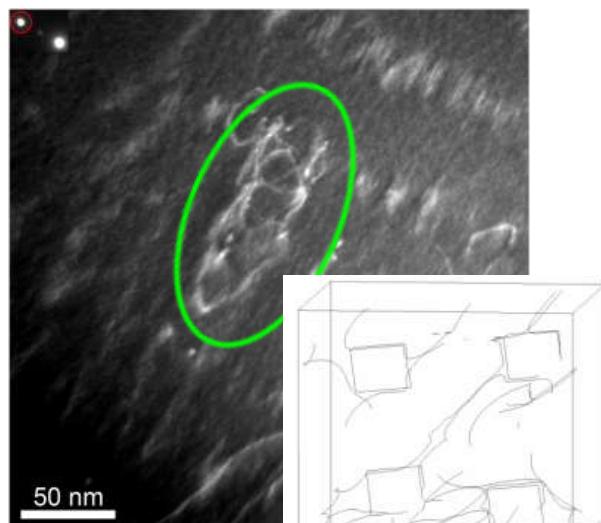
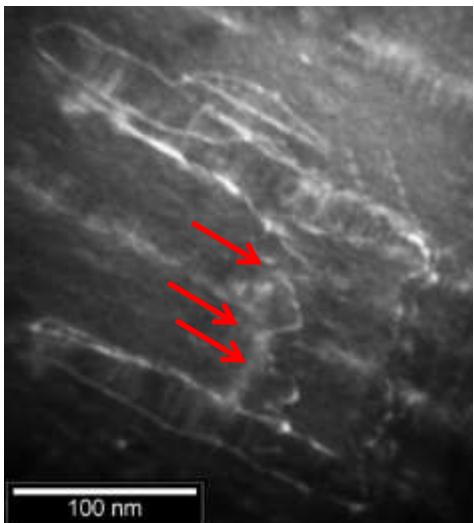
40 nm

•C ■ ≥ 7.0 at.% C



Weight reduced steels

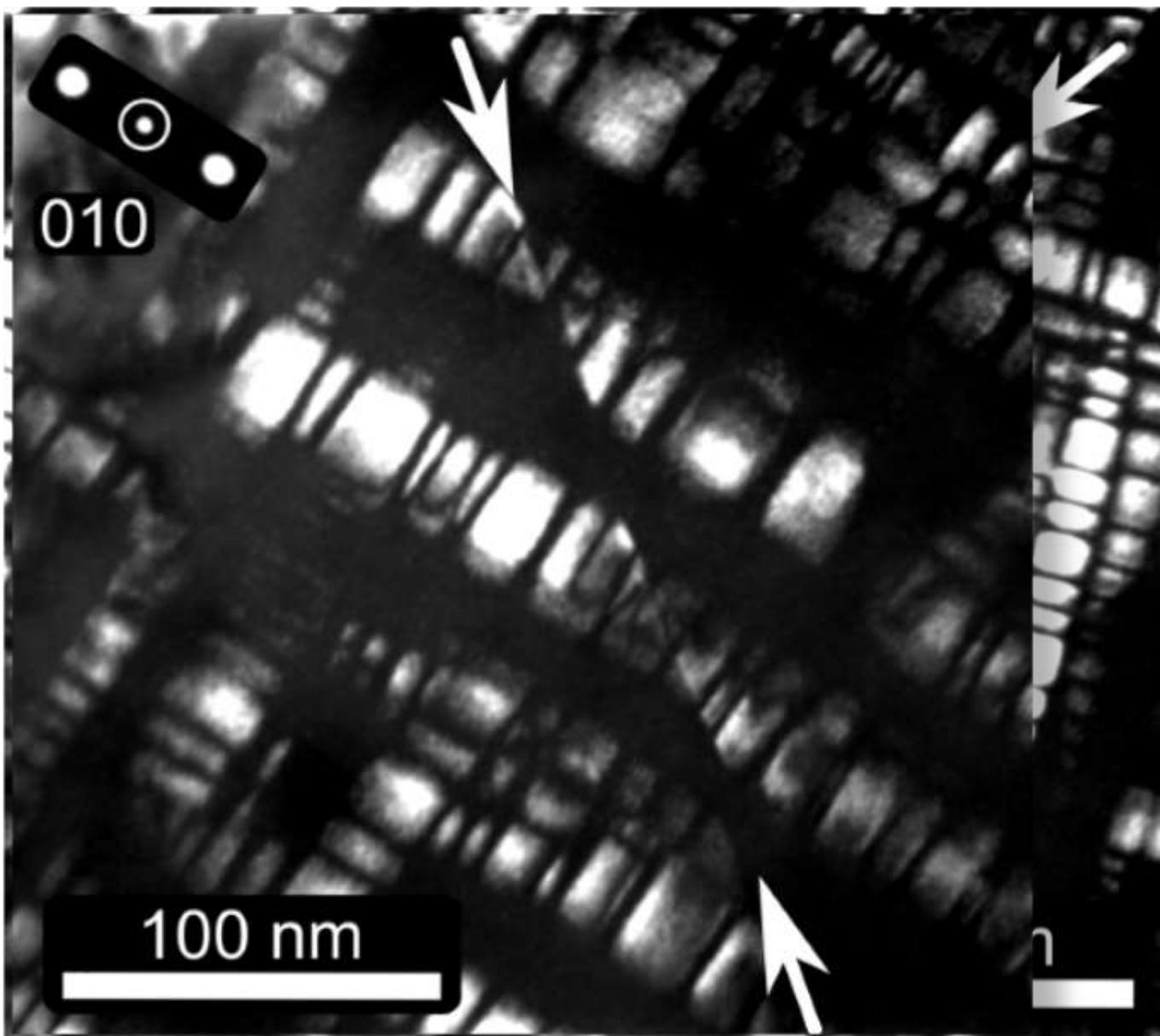




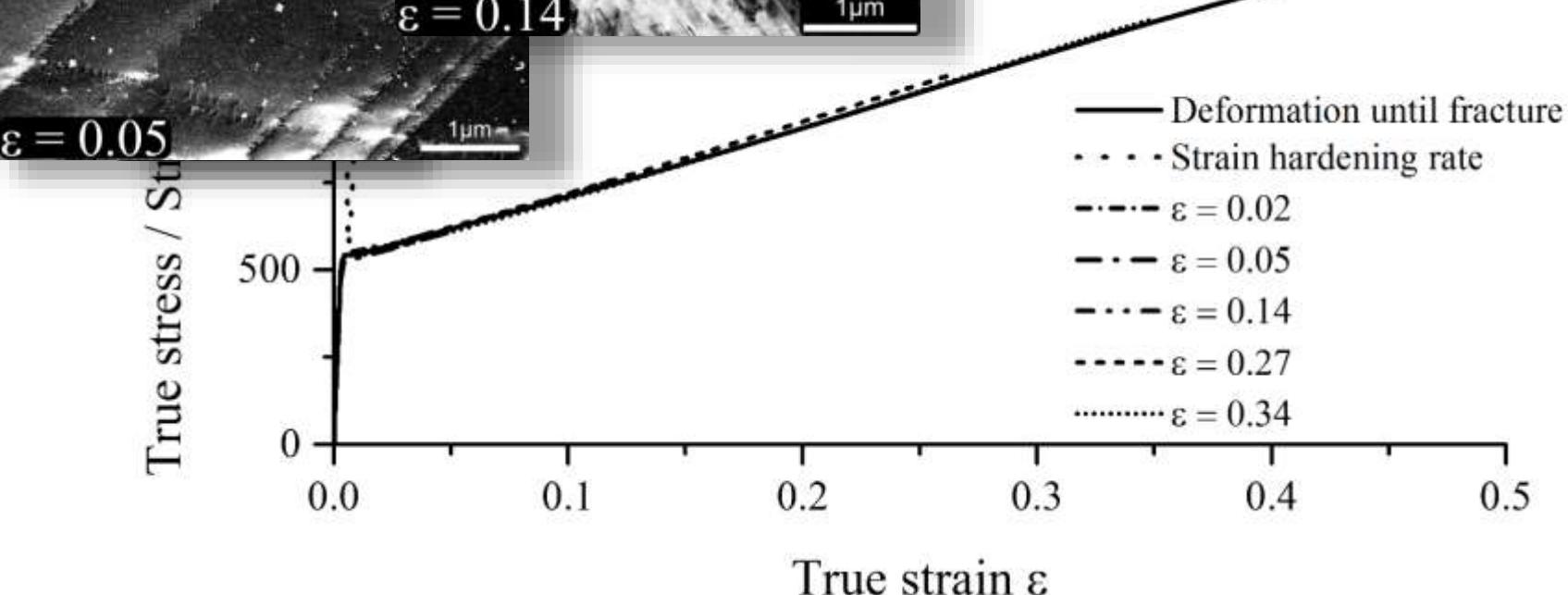
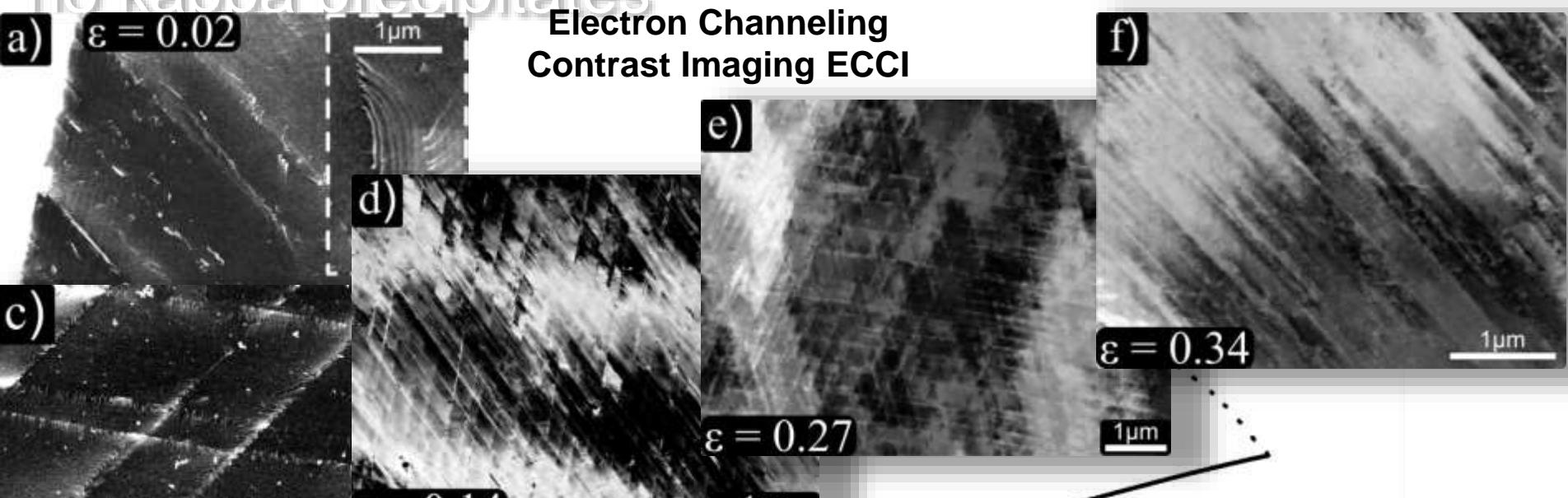
Dislocation pinning due to cross-slip into different conjugate glide plane

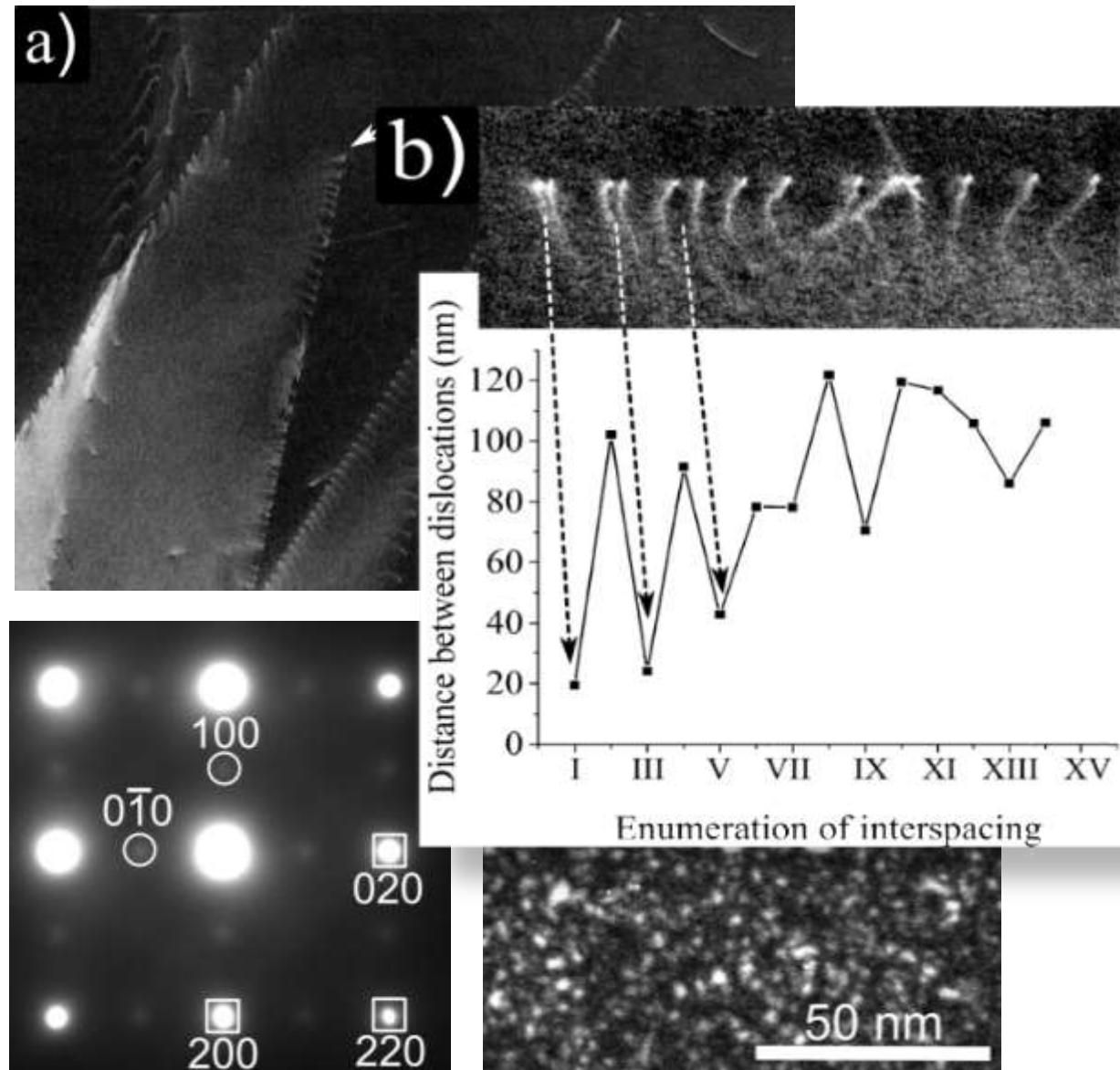
Dislocation wrapping around κ -carbides

Formation of slip bands from individual dislocation sources

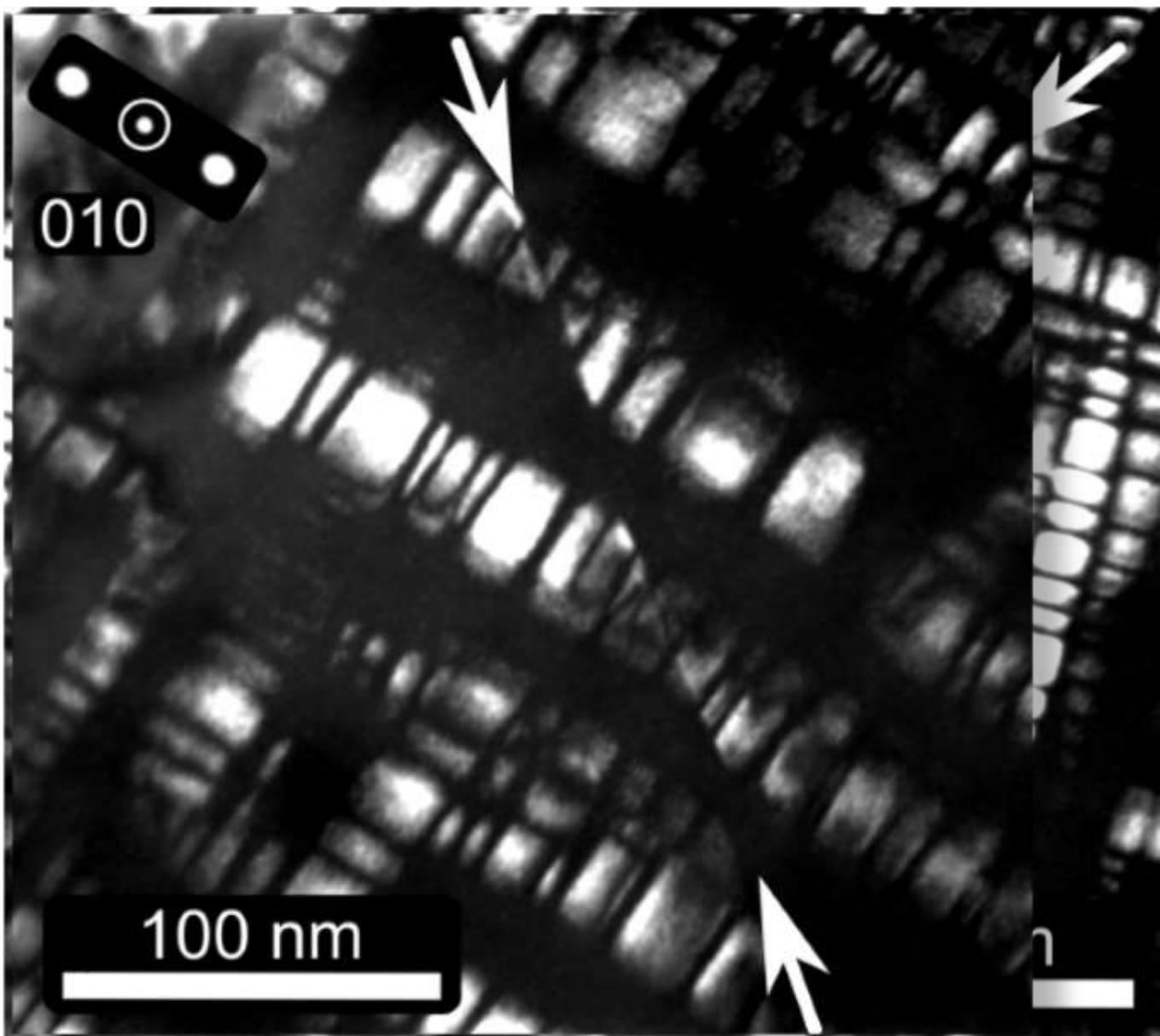


$_{5}$ Fe-30Mn-8Al-1.2C (wt%), as-quenched, no kappa precipitates





Electron Channeling
Contrast Imaging ECCI



$$\sigma_{\text{SH}}(\varepsilon) = K \cdot M \cdot G \cdot b/D$$

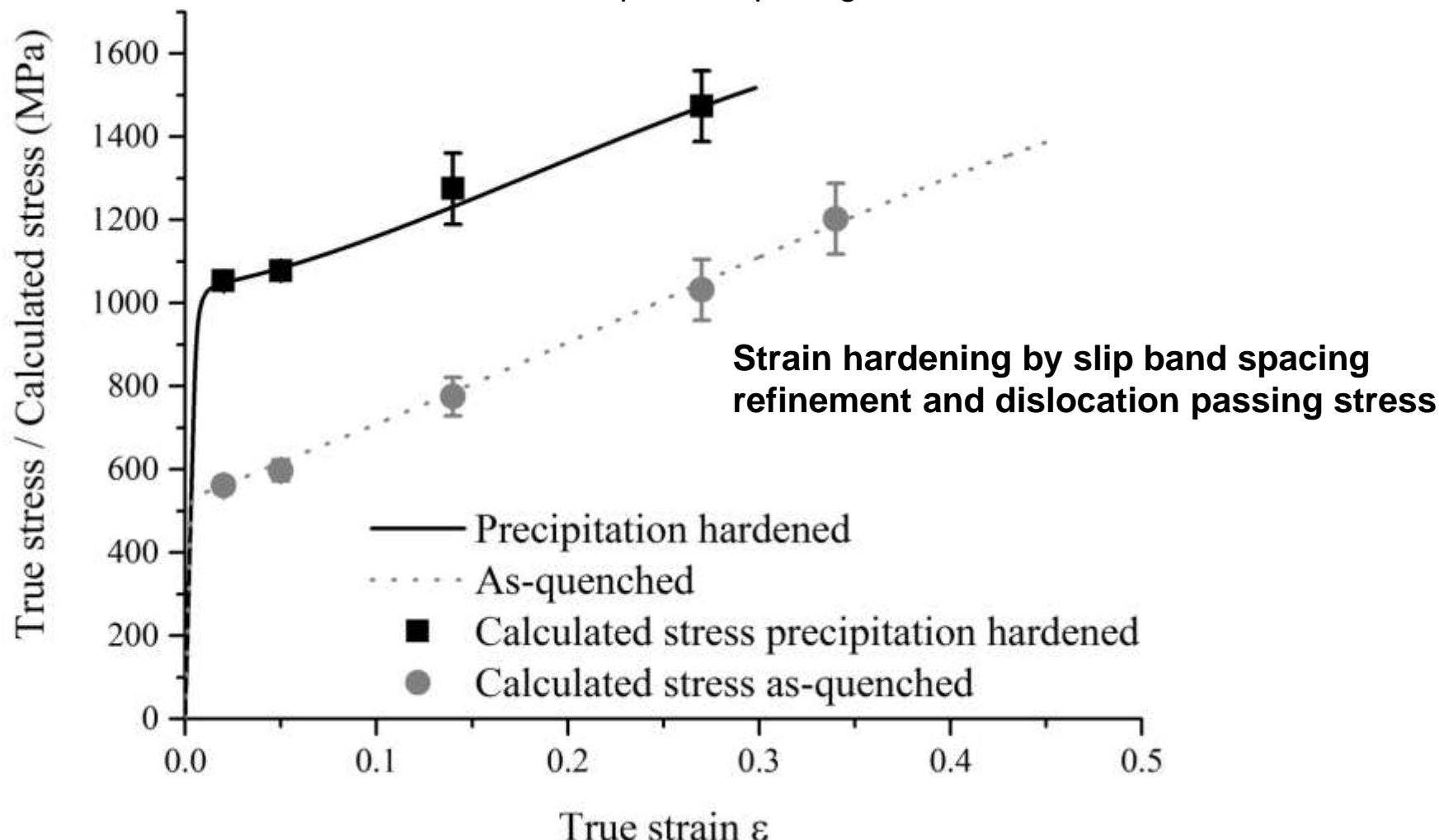
K : geometrical factor

G : 70 GPa

M : 3.06 Taylor-factor

b : 0.26 nm

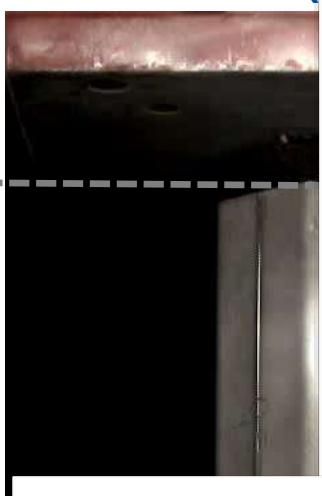
D : mean slip band spacing



Strain rate 800/s: compare TWIP steel to DP800

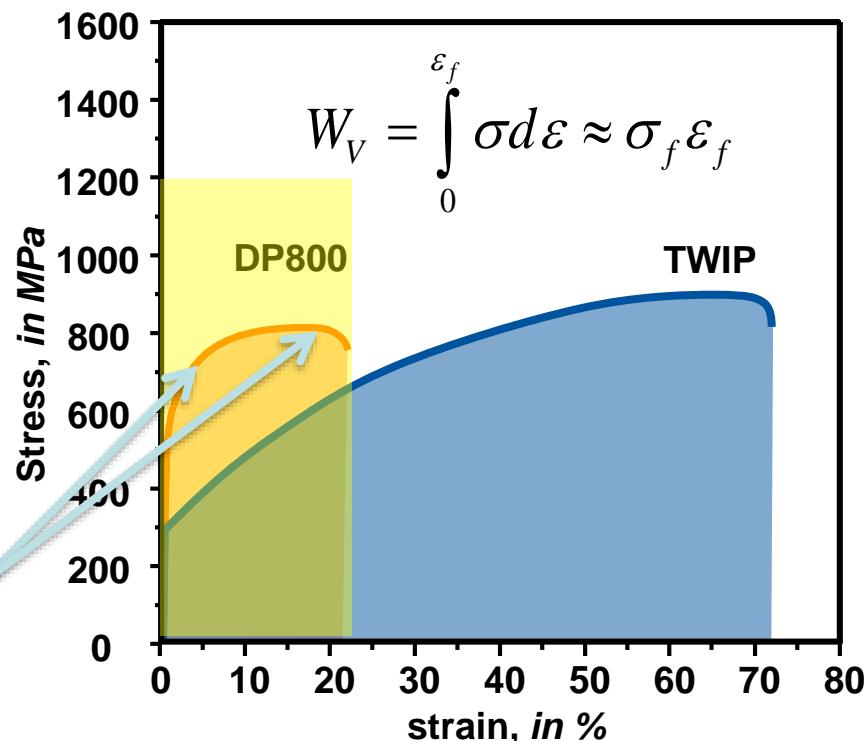


TWIP (

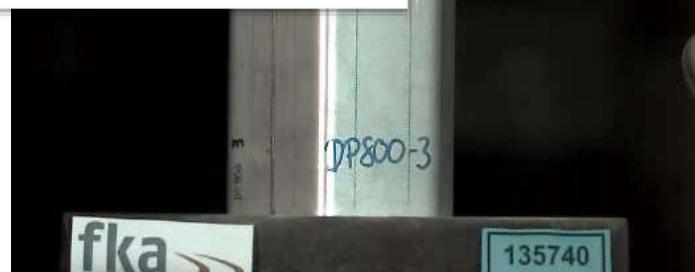
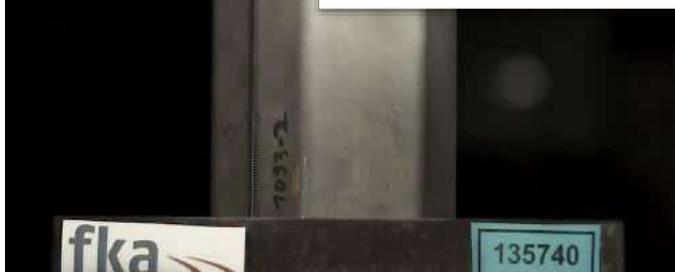
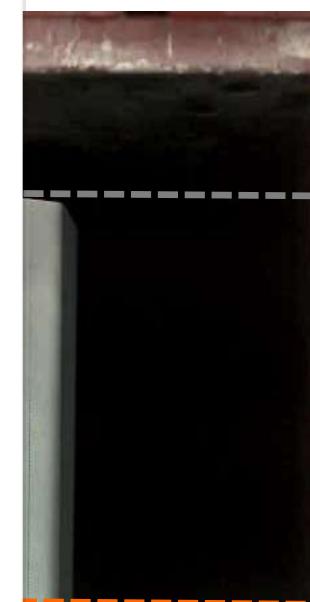


165 mm

Loading
points from
buckling



0



DFG SFB 761: M. Bambach, G. Hirt (RWTH)

1. What is Metastability Alloy Design and Segregation Engineering ?

2. How is it done ?

- Bulk: tune barriers & transformation driving forces
- **Confinement to lattice defects**
Segregation & local displacive transformation

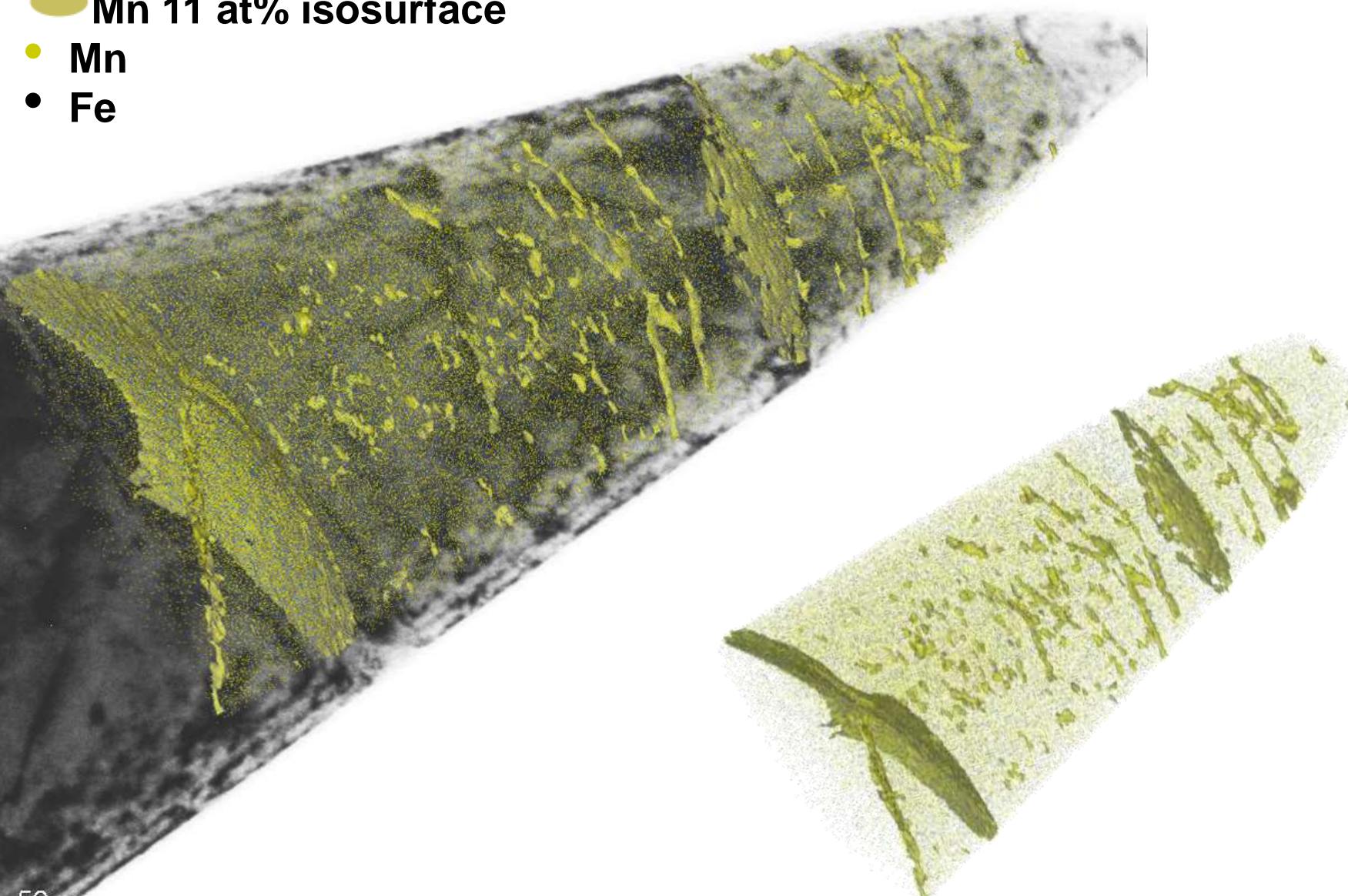
Fe-9%Mn, 450°C/6h



Mn 11 at% isosurface

Mn

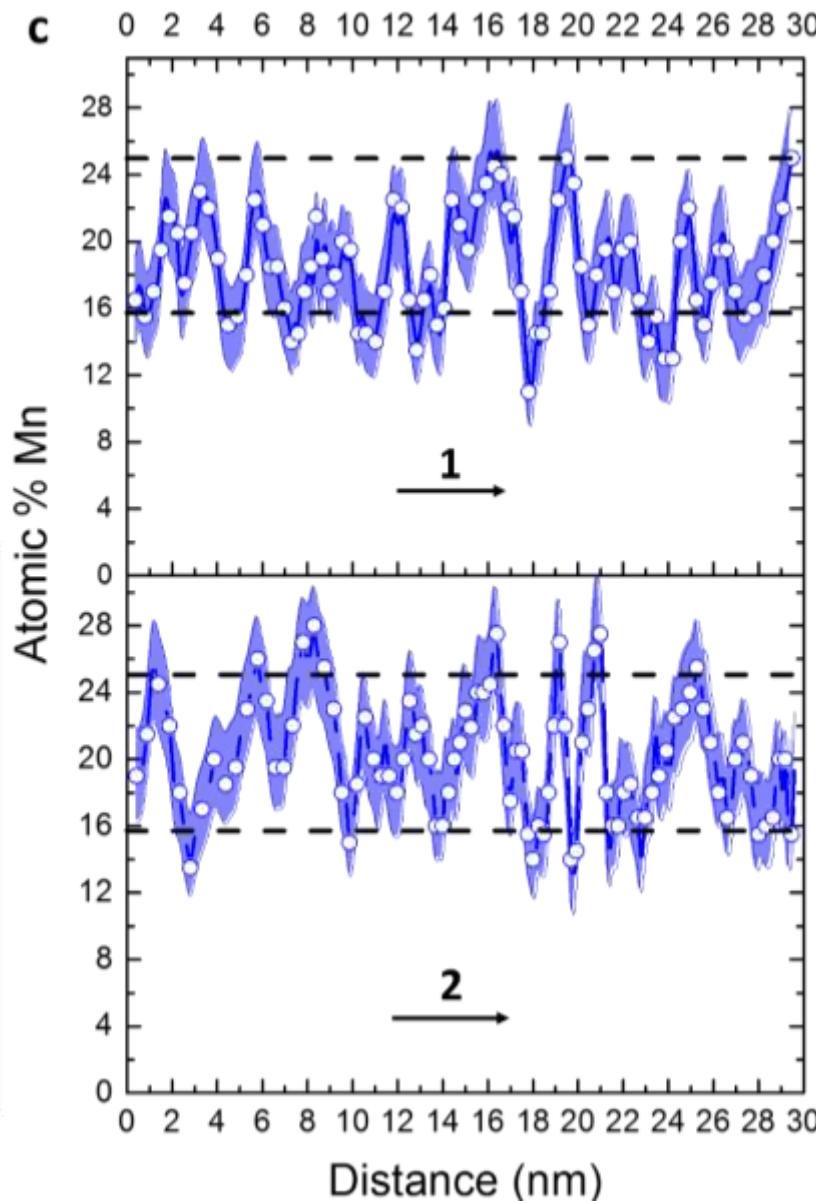
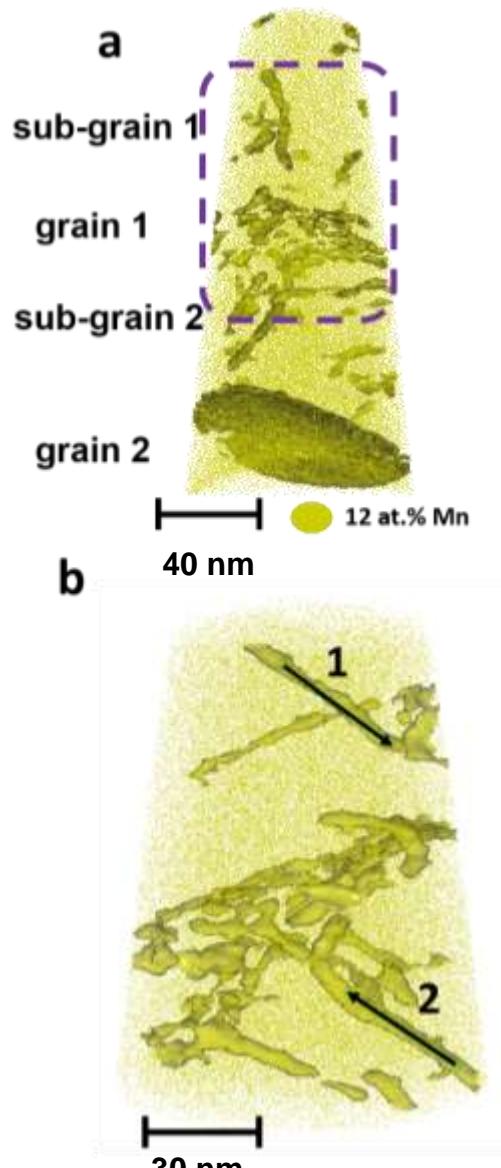
Fe



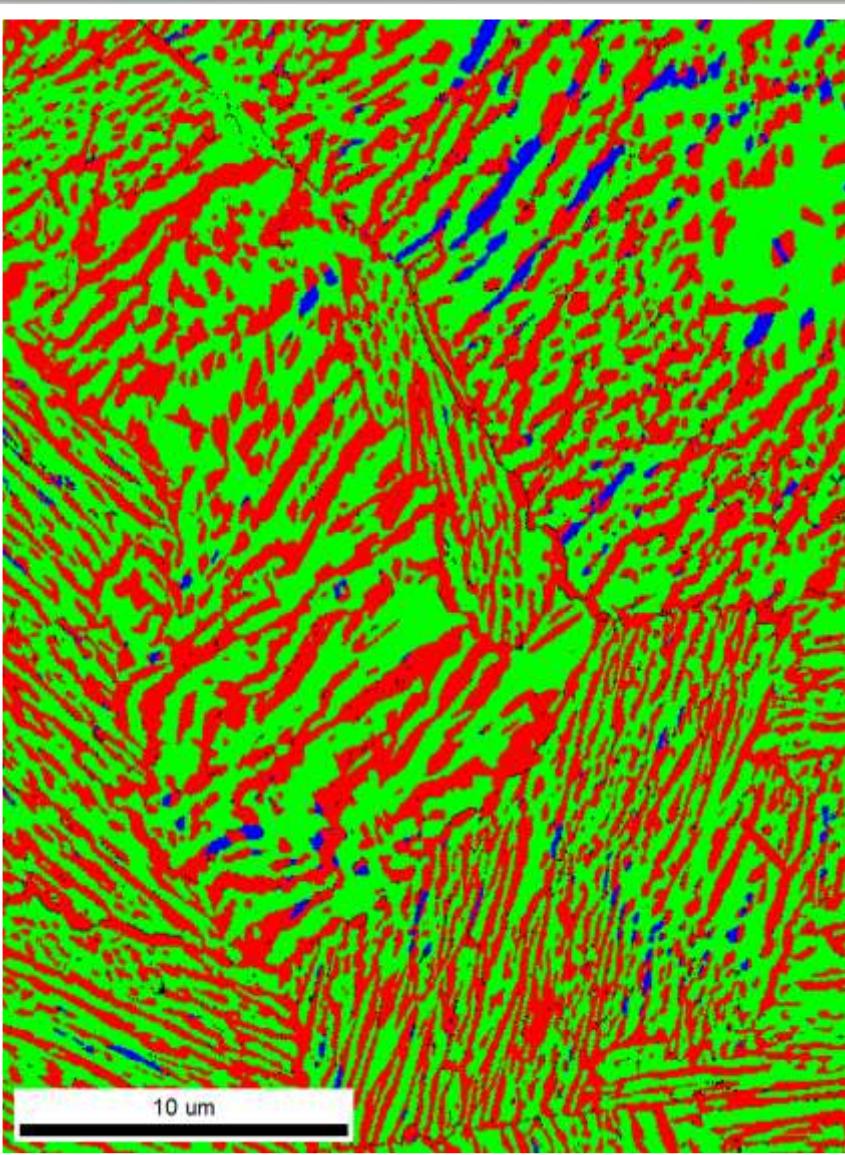
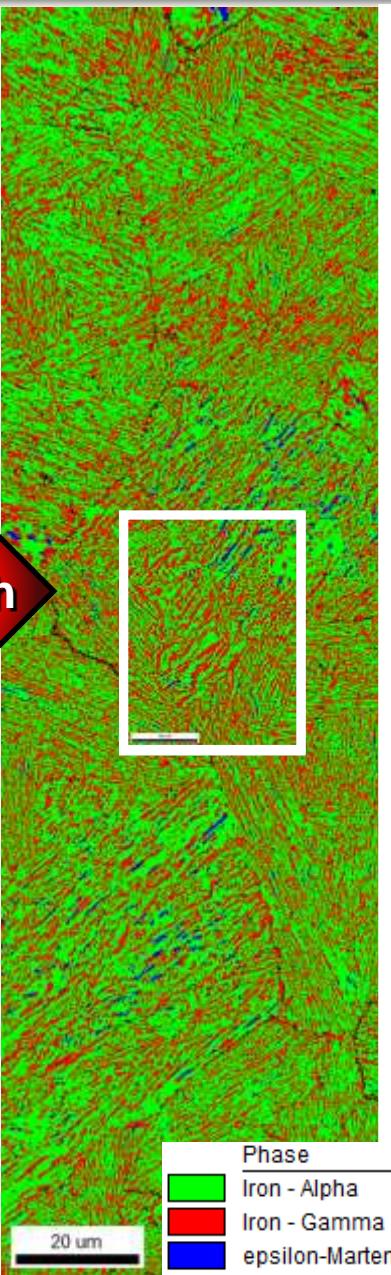
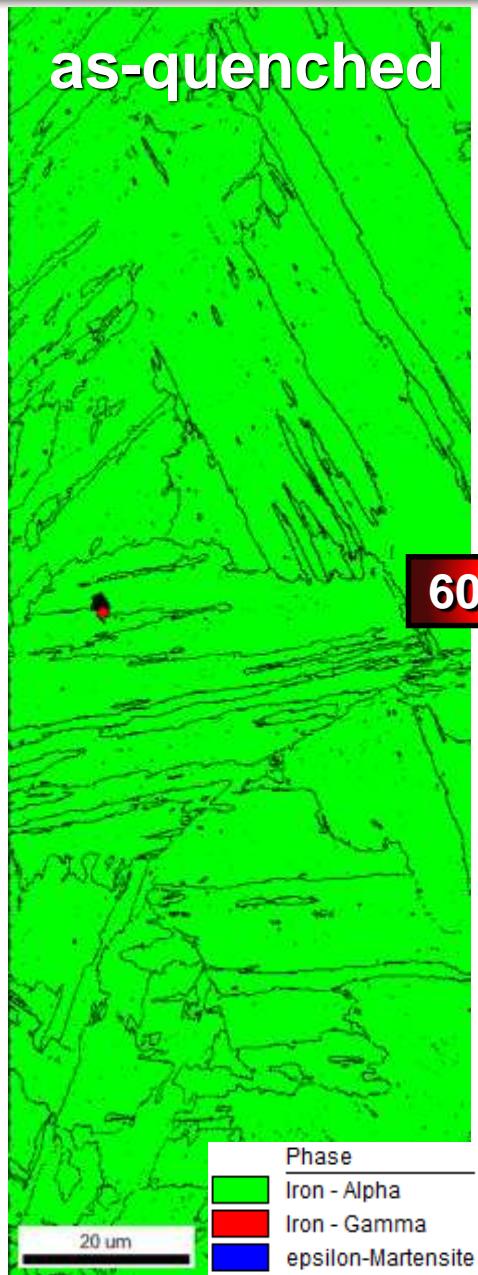
Fe-9%Mn 450°C/6h, dislocation spinodal



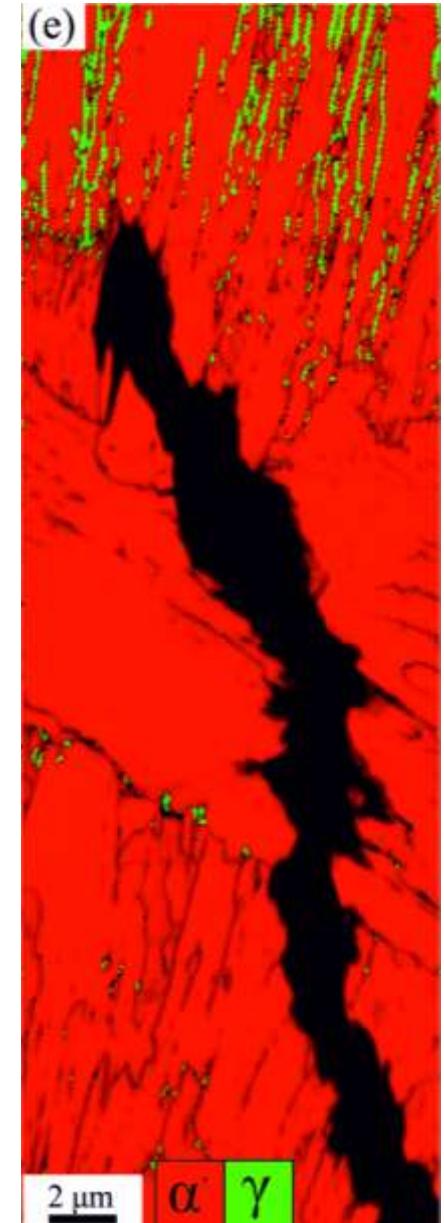
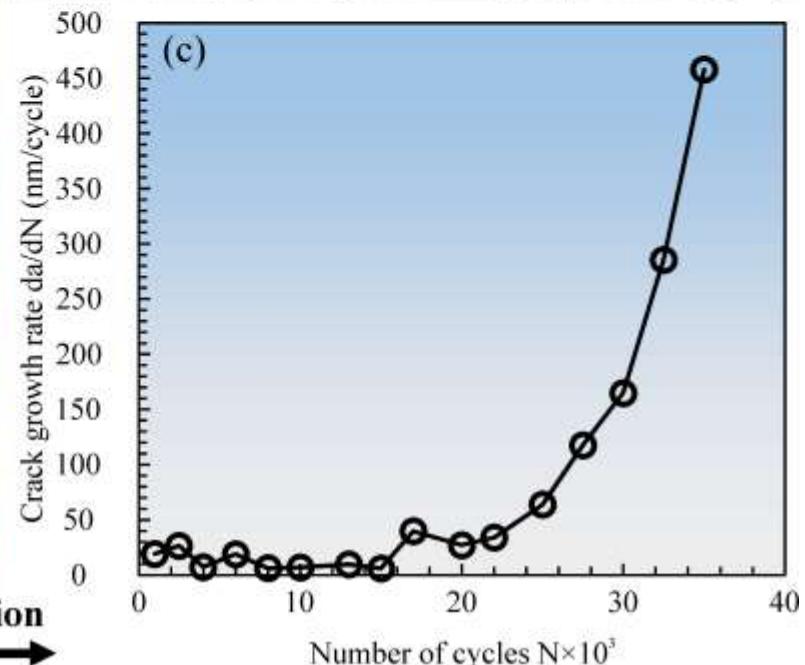
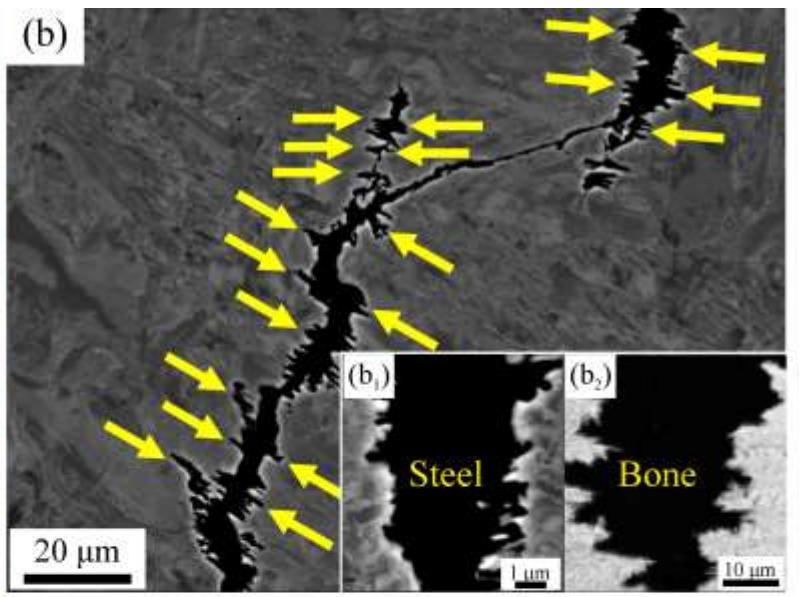
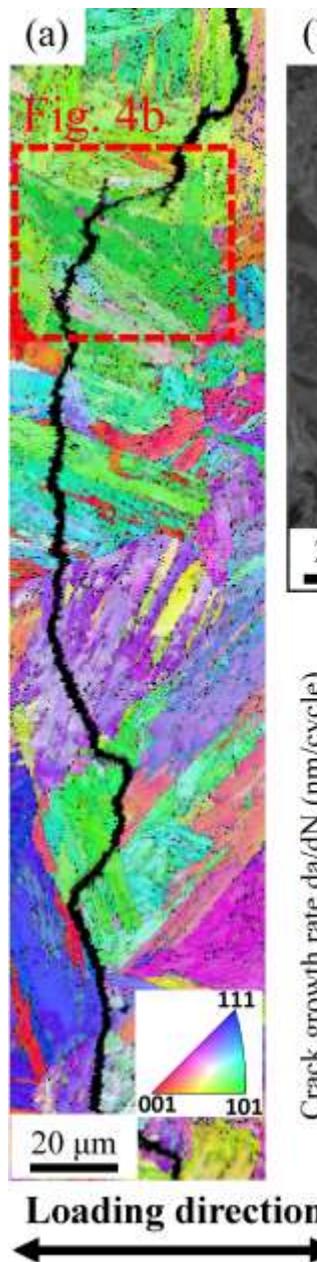
YEARS 1957-2017
100



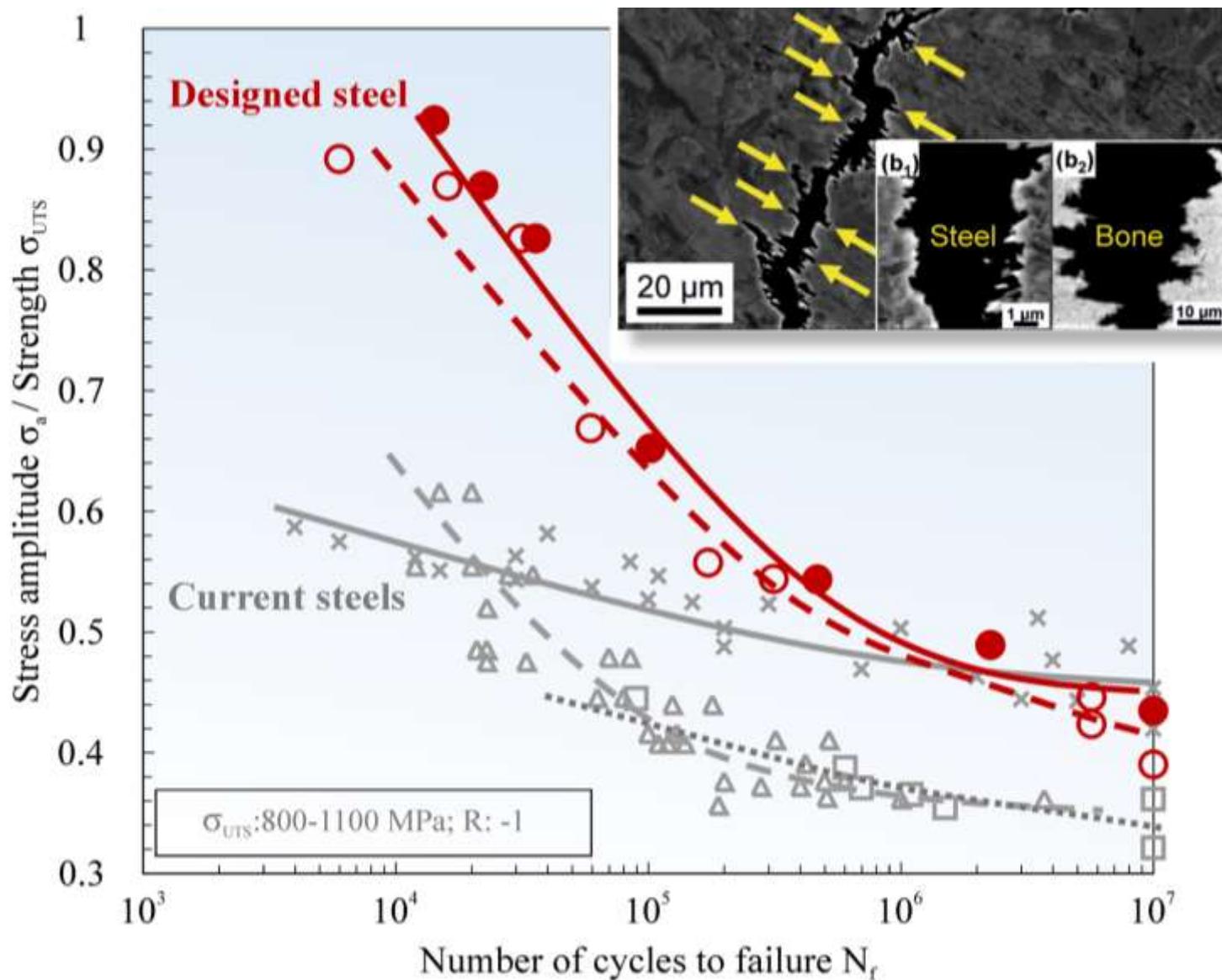
Austenite films in Fe-9Mn-3Ni-1.4Al (wt%): reversion steels



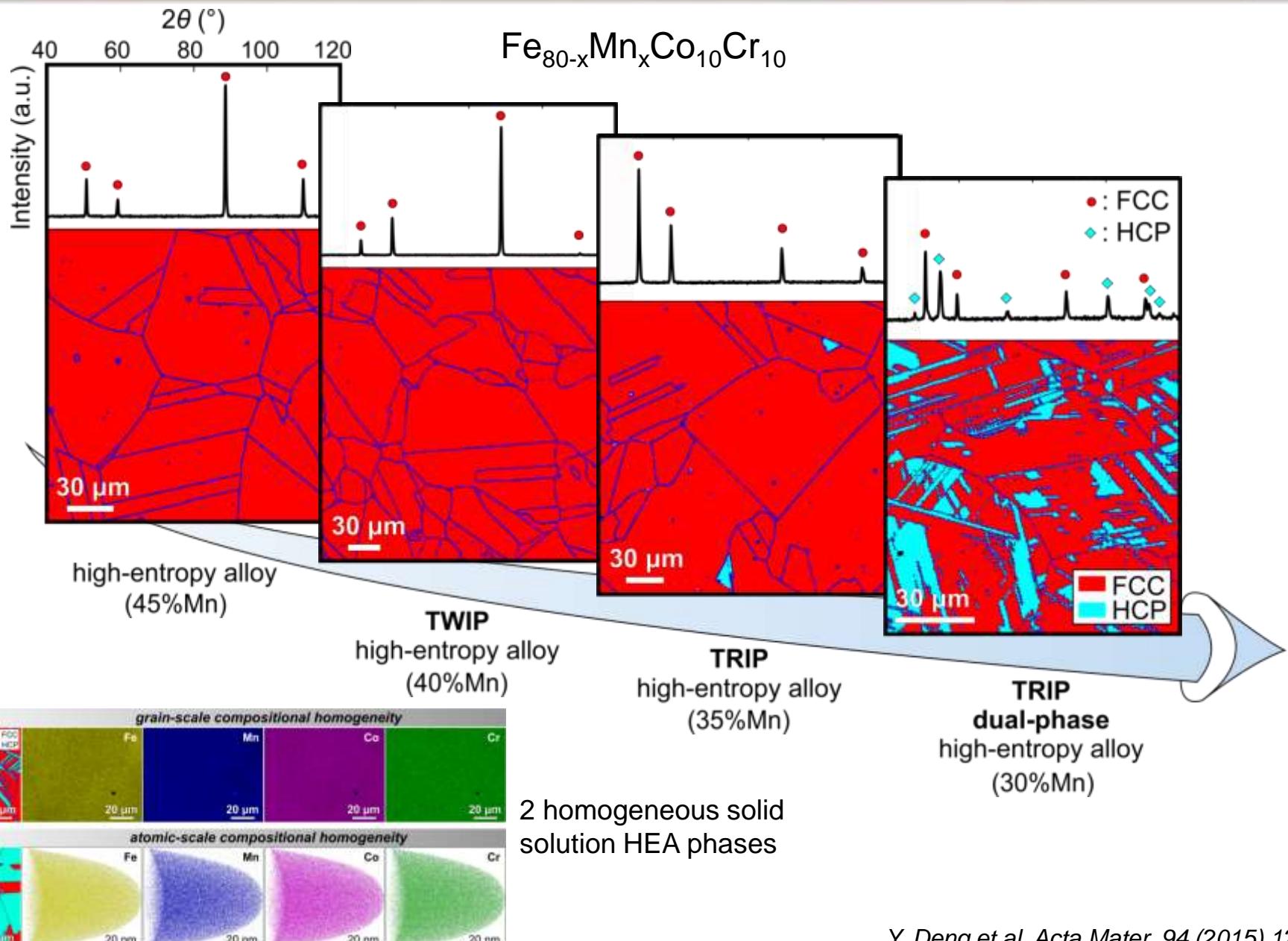
Metastability alloy design towards bone – like metals



Metastability alloy design towards bone – like metals

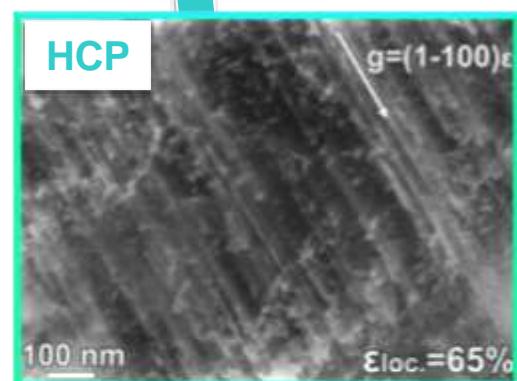
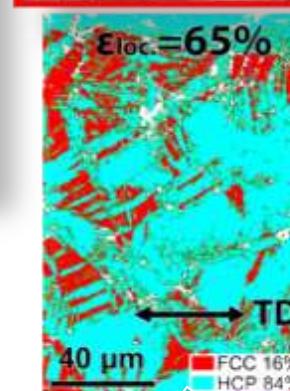
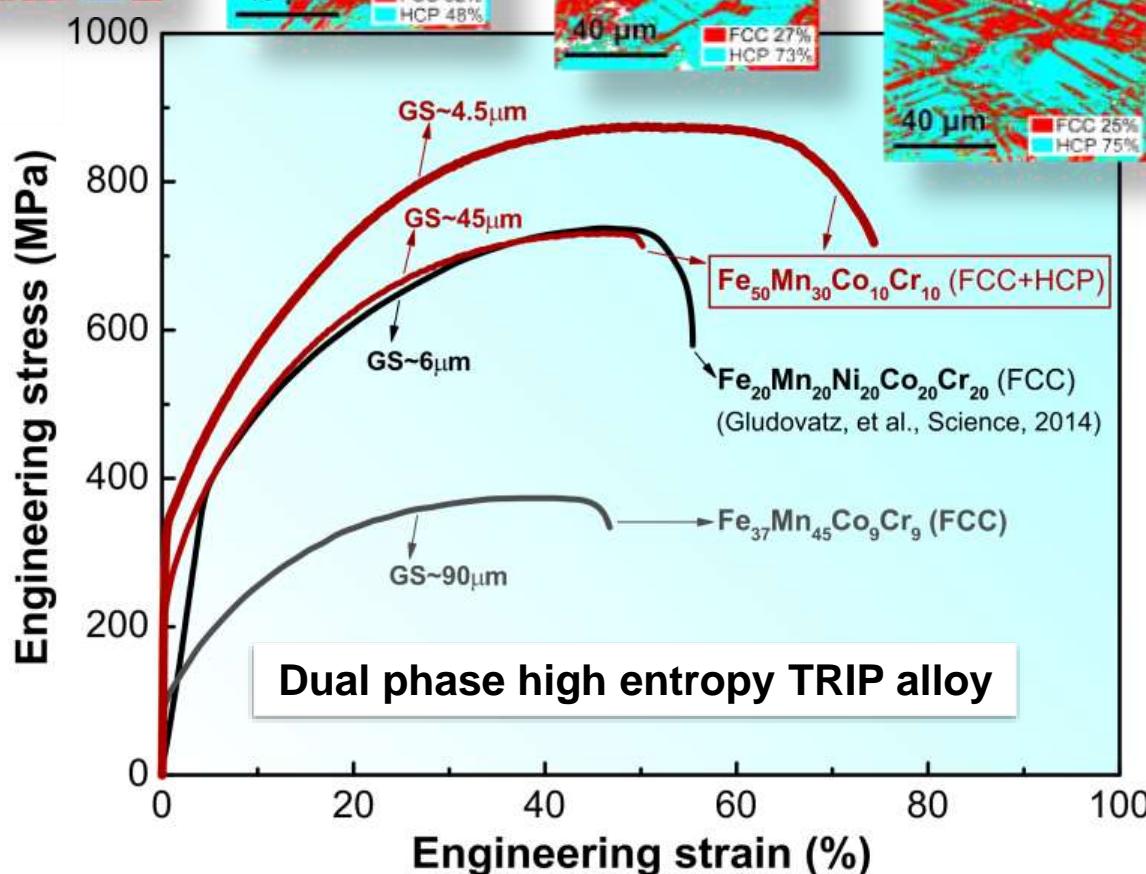
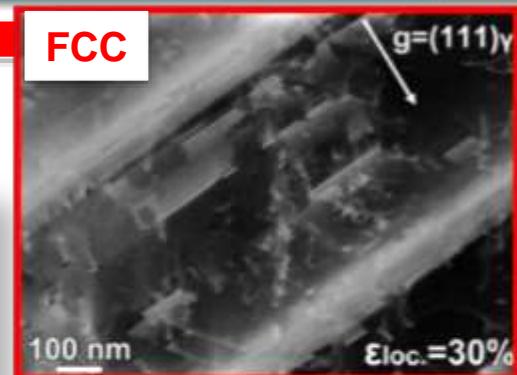
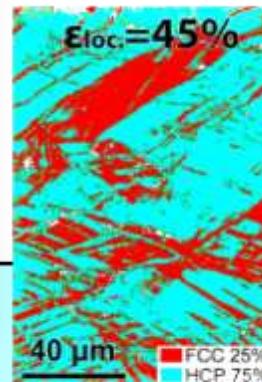
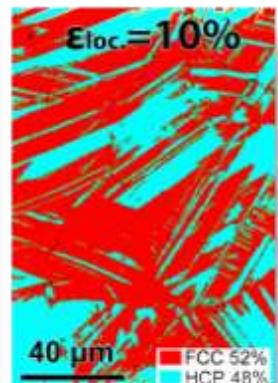


Theory-guided design: non-iso concentration high entropy alloys



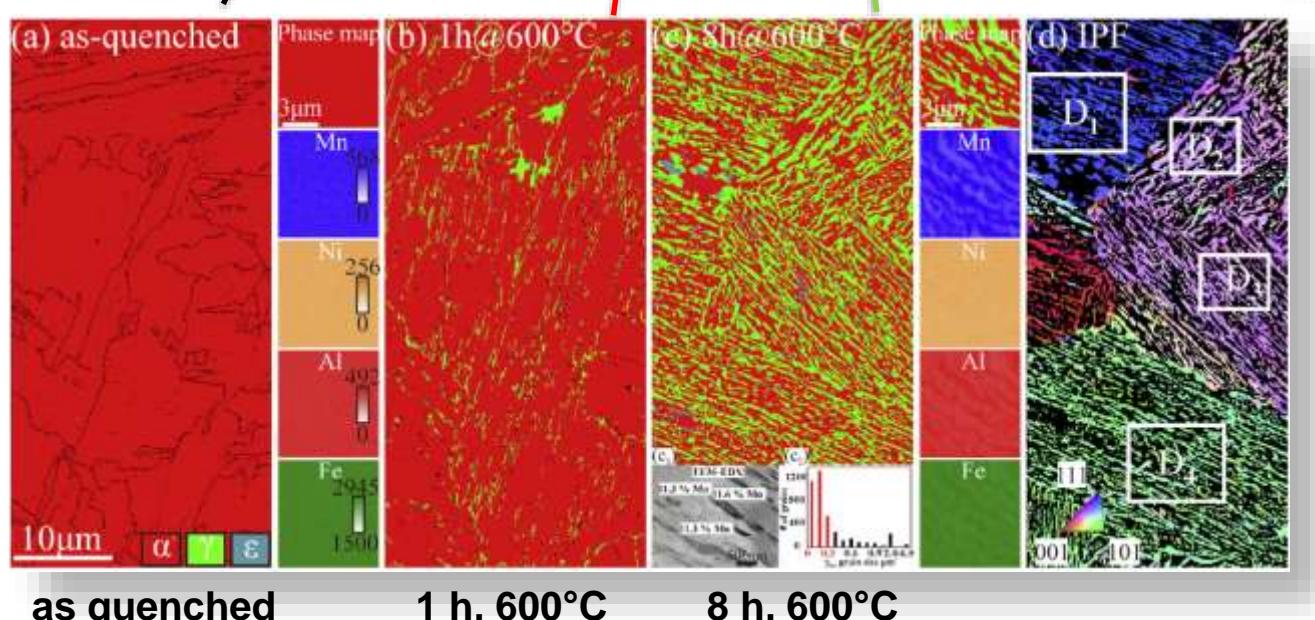
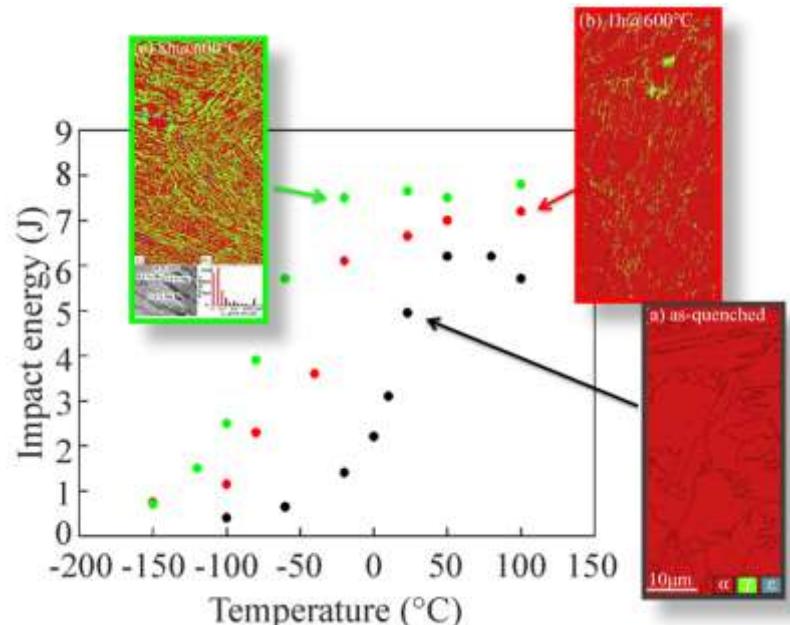
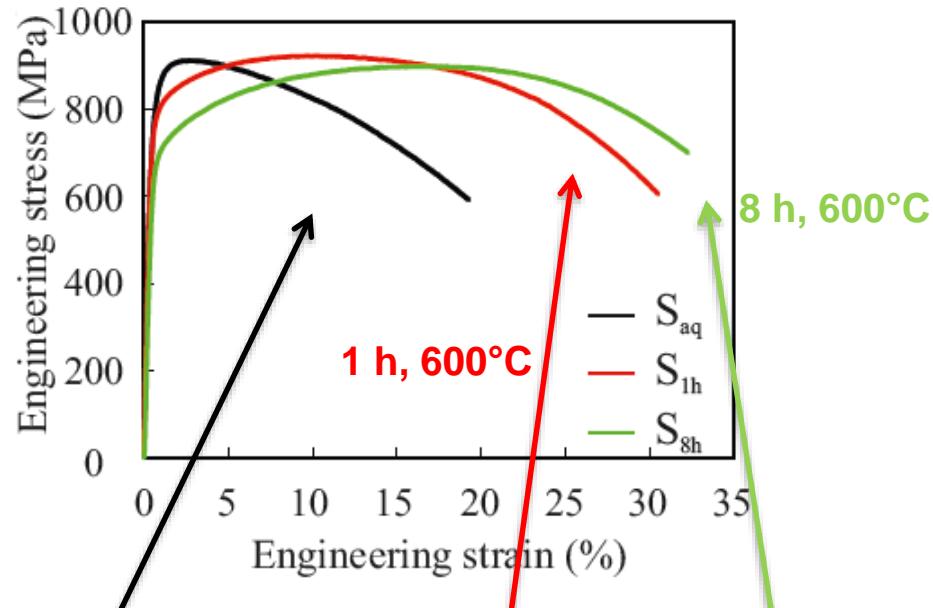
2 homogeneous solid solution HEA phases

Theory-guided design: non-iso concentration high entropy alloys



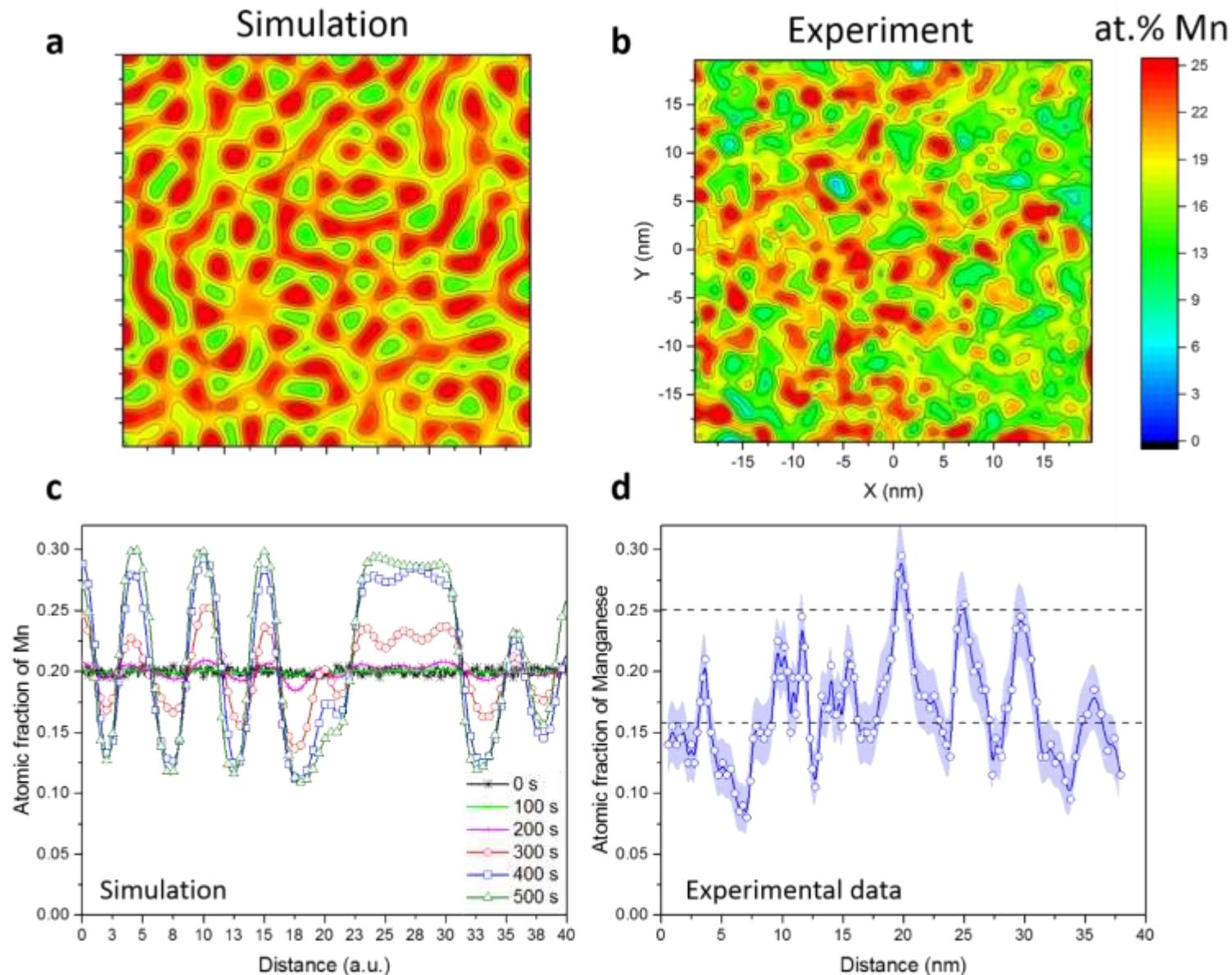
Z. Li et al. *Nature* 2016

Nanostructured bulk alloys by phase reversion: towards properties

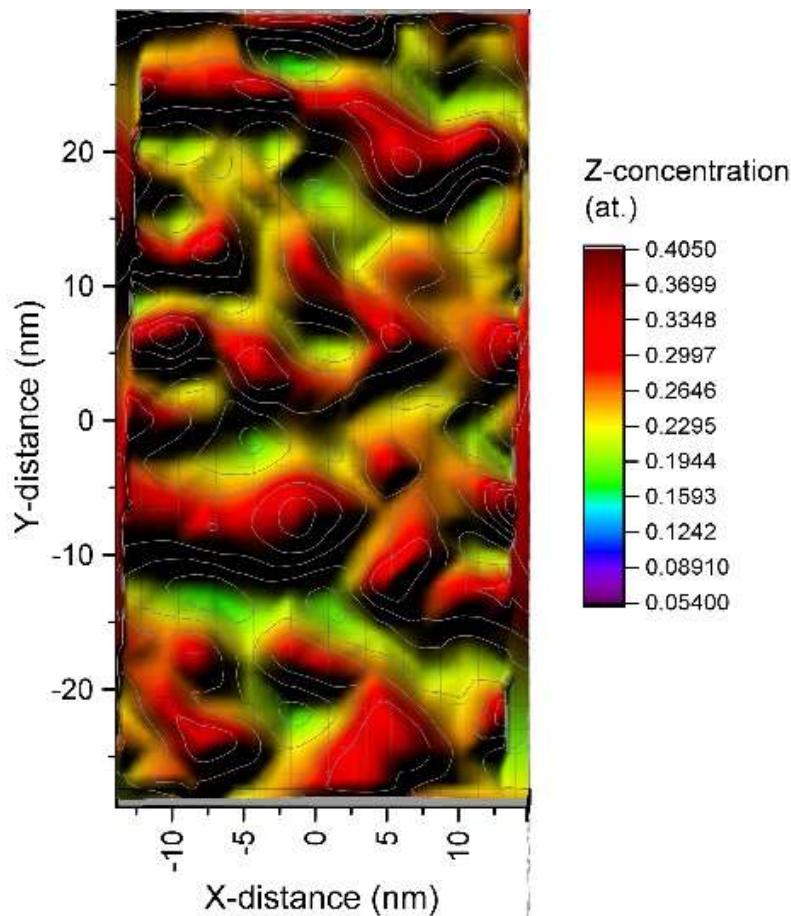


Wang et al. Acta Mater. 79 (2014) 268;
Dmitrieva et al. Acta Mater. 59 (2011) 364

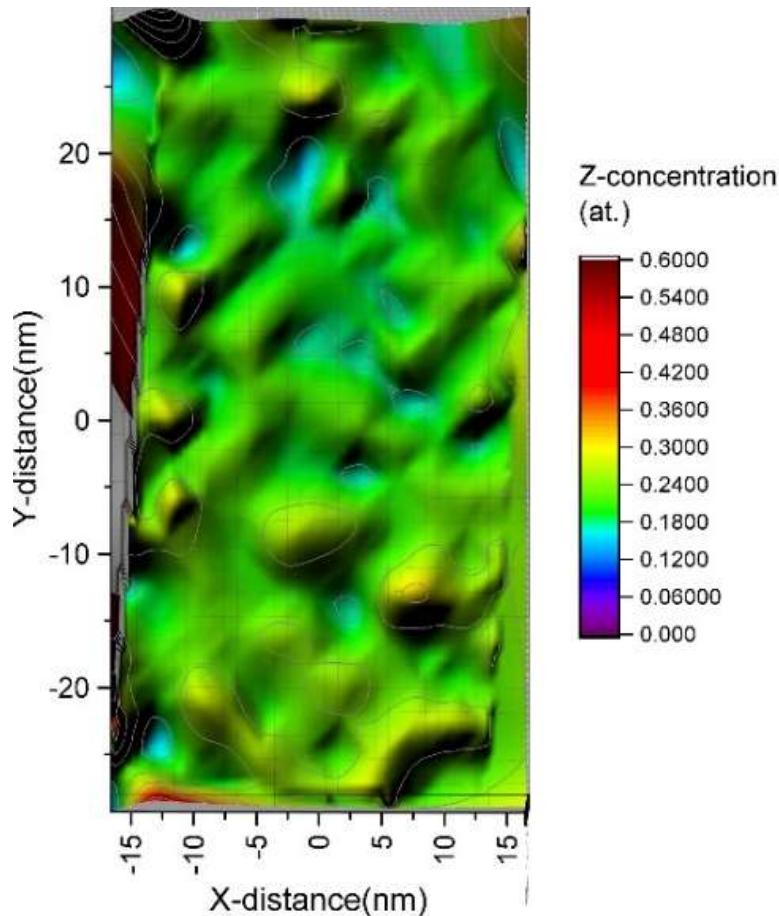
Grain boundaries in Fe-9Mn

YEARS 1917–2017
100

GB co-segregation in Cantor HEA

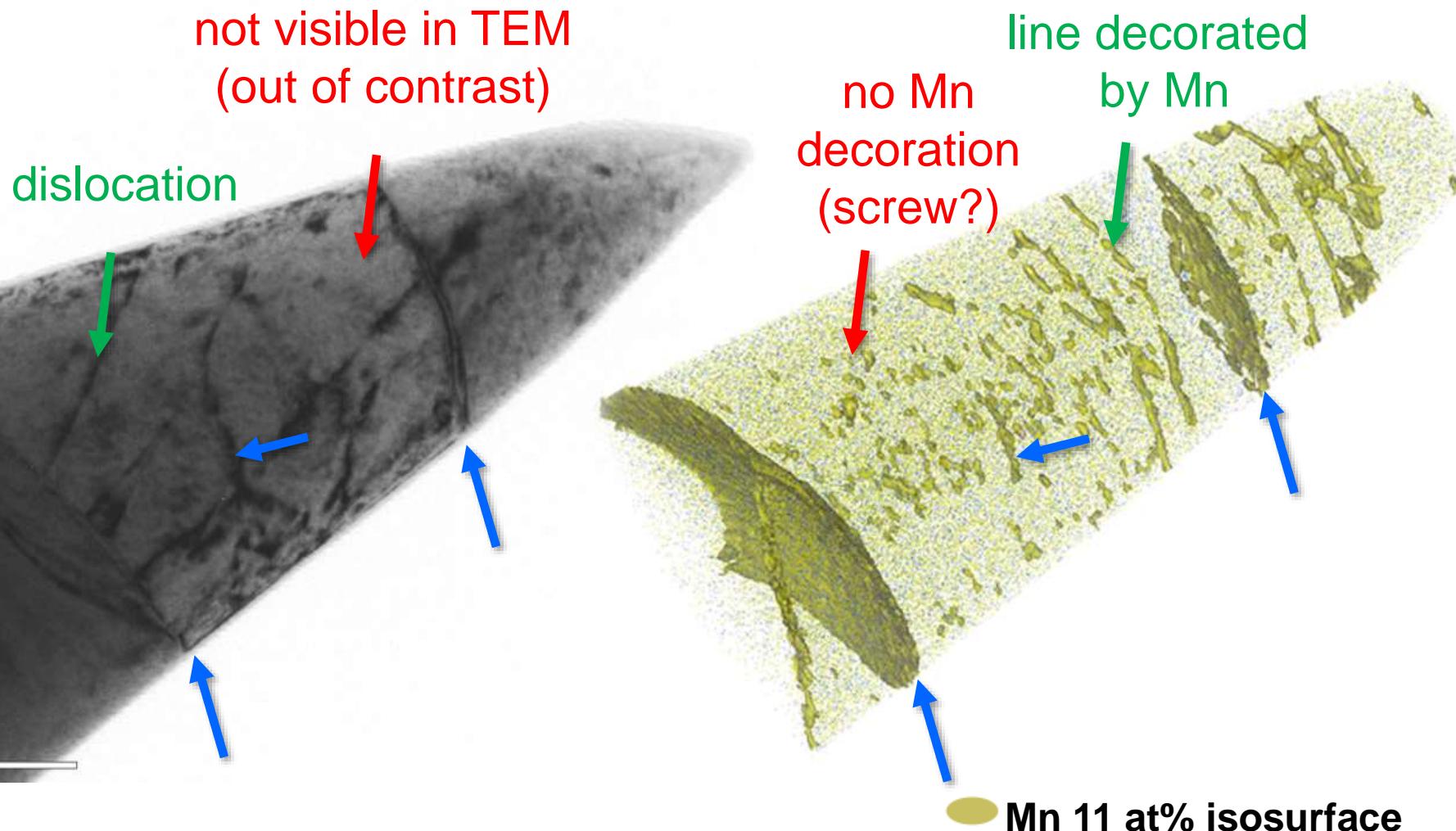


Ni in GB
450°C, 6h



Mn in GB
450°C, 6h

Grain boundaries and dislocations visible in both, TEM and APT



20 nm

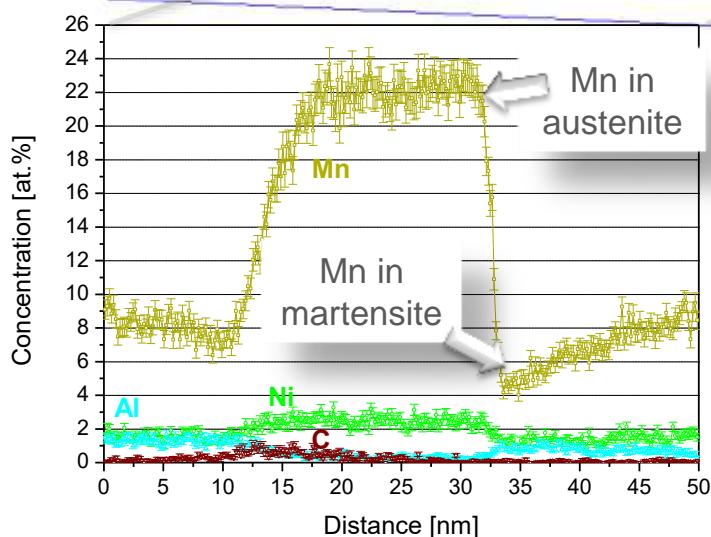
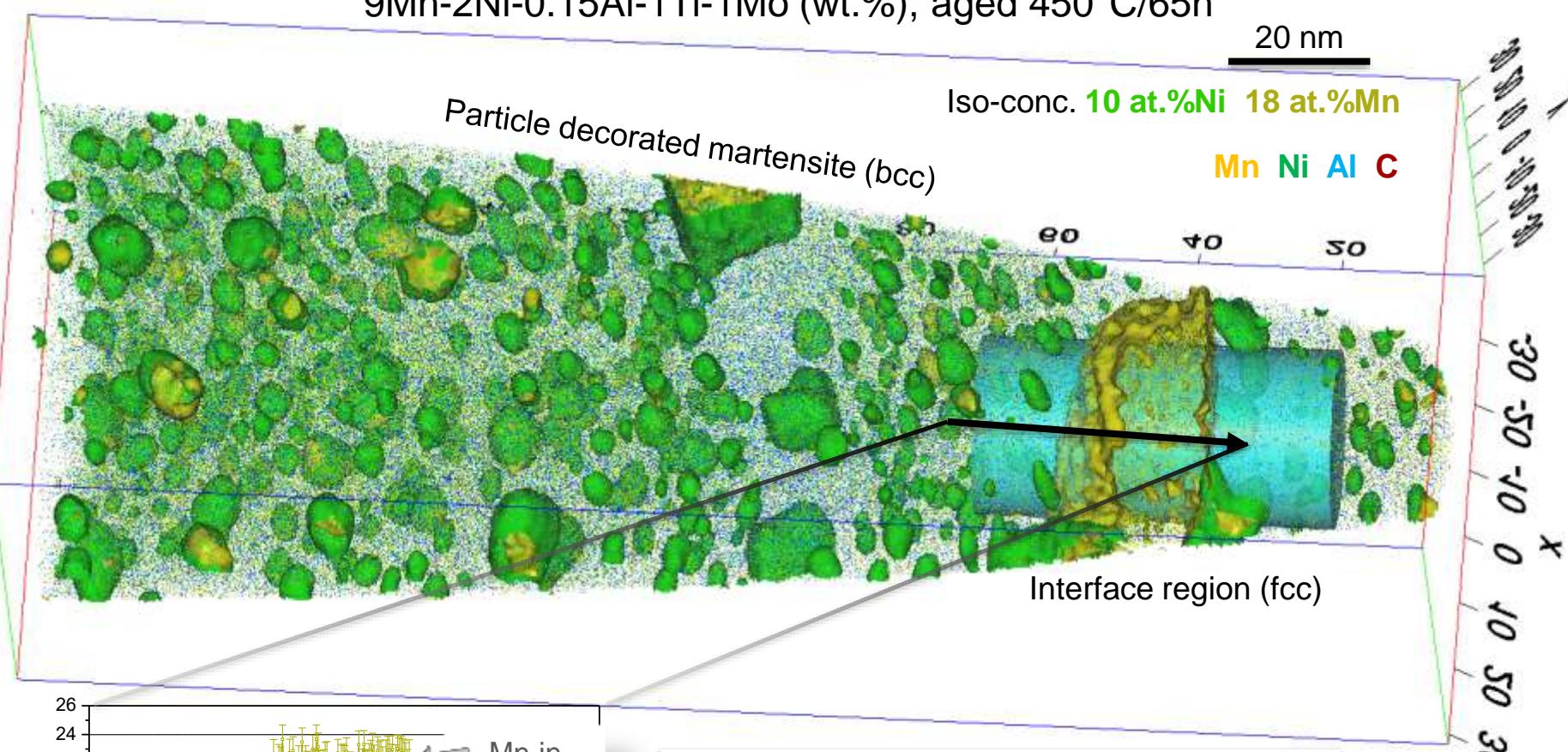
Particle decorated martensite (bcc)

Iso-conc. 10 at.%Ni 18 at.%Mn

Mn Ni Al C

Interface region (fcc)

x



Phase formation at martensite interface

